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25 YEAR RE-REVIEW

## HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT, U. S. A.

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1.0 GENERAL IMPORMATION

1.1 SCOPE

This Specification covers the performance requirements for the model JFC-47 Main Engine Control independent of Main Engine Pump.

1.1.1 DESCRIPTION OF COMTEMES

The Test Requirements in this specification are divided into four basic sections as follows:

I. Pre-hot test performance
II. Hot test
III. Final Data
IV. Audit

The tests outlined in section I are required in order to define the performance of the control after all systems have been adjusted and calibrated to ensure that the unit is functioning satisfactorily before hot testing.

The tests in section II are comparative fuel temperature tests. These tests will define high temperature performance and schedule shifts as a function of fuel temperature changes.

The tests in section III define the control performance and accuracies of the entire map of control functions.

The test in section IV is a check to determine control repeatability and integrity.

- 1.2 <u>Equipment Required</u>
- 1.2.1 A flow bench with Main Pumps capable of supplying PMC9073 Fuel at the rate of 40 000 pph at 1000 psi, maintaining a fuel temperature of
- 1.2.2 A drive capable of driving the control at 0-4600 RPM, with 1/2% regulation; 1/4% drift. Drive must be capable of setting speed within ±2 RPM. Speed indication must be within ±1 RPM.
- 1.2.3 A presumatic pressure and vacuum source capable of maintaining any pressure from 2 to 200 psia, to simulate engine burner pressure (Pb).

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- 1.2.4 A pneumatic pressure and vacuum source capable of maintaining any pressure from 1 to 50 psia, to simulate engine inlet pressure (Pt2).
- 1.2.5 Thermocouples and an indicating unit with ±3°F accuracy for measuring temperatures between -65° and +300°F, and ±5°F accuracy between 300° and 900°F.
- 1.2.6 Flowmeters

Metered Flow 1000 - 40,000 PPH ±1/2 Accuracy Total Flow 1500 - 40,000 PPH ±1/2 Accuracy Transducer Flow 100 - 1,000 PPH ±1% Accuracy

#### 1.2.7 Pressure Gages

O-2000 psi ±1% Accuracy Control Inlet 0-1000 psi ±1% Accuracy Control Discharge 10-50 psi ±1% Accuracy 0-300 psi ±1% Accuracy Throttle Valve Differential Control Body 0-1000 psi ±1% Accuracy Afterburner Signal Area Control Inlet 0-1500 psi ±1% Accuracy 0-1000 psi ±1% Accuracy Area Control Metered 0-50 psia ±.25% Accuracy Compressor Inlet C-200 psia ±.25% Accuracy Burner 0-1000 psi ±1% Accuracy Main Shutoff Valve Signal 0-1000 psi ±1% Accuracy Recirculating Valve Signal 0-100 psi ±1% Accuracy Pump Inlet

- 1.2.8 A system shall be provided to maintain the control discharge pressure within 10% of curve number 1.
- 1.2.9 Torque measuring equipment to read torque (10-100 in-1bs.) at the CBA shaft. Readings shall be accurate to ±3 in-1bs. A protractor is required to measure rotation of CBA shaft (60° total).
- 1.2.10 Torque measuring equipment to read torque (0 30 inch-pounds) at the power lever with an accuracy of tl in-lb.
- 1.2.ll A power lever protractor which will allow reading and setting the power lever to any desired angle between -10° and 130° and reading the angle to an accuracy of 1/2°.
- 1.2.12 An adjustable stop shall be provided to satisfy the requirements of paragraph 11.1.

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- 1.2.13 At the room temperature, rig temperature baths or an oven are required to set Tt2 at the following temperatures: -65°F, 0°F, +59°F, 150°F, 250°F, 300°F, 415°F, 550°F, and 750°F. Temperature control must be maintained within +2°F up to 200°F and within +1% above 200°F.
- 1.2.14 Pressure relief valves shall be incorporated to limit inlet pressure (Pf2) to 1200 psi maximum and body pressure (Pfl) to 260 psi maximum.
- No, Tt2, and Pt2 servo position indicating fixtures with a range of 1.50 inches 1.2.15 reading in increments of .001 maximum.
- 1.2.16 Fixed Orifices
- 1.2.16.1 Orifice "W" (Reference Figure 2 and Paragraph 9.4) .0325 + .0025 diameter.
- 1.2.16.2 Orifice "X" and Valve A (Reference Figure 1 and Paragraph 11.1.1) Set for 620  $\pm$  5 pph at 500  $\pm$  5 psi  $\triangle$  P (P<sub>h</sub> - P<sub>m</sub>) with Valve A wide open.
- 1.2.16.3 Orifice "Y" (Reference Figure 1 and Paragraph 11.1.1) Set for 620 + 5 pph at 67 ± 5 psi \( P\_h - P\_t \).
- 1.2.16.4 Orifice "Z" (Reference Figure 3 and Paragraph 11.5.1) Set for 75 + 10 pph at 150 + 10 psi A P.
- 1.3 Hot Test Equipment
- 1.3.1 A flow bench similar to that required in Paragraph 1.2.1 but capable of operating at 450°F with P&WA 523 Fuel.
- 1.3.2 An oven capable of varying Tt2 temperature on the sensor bulb from  $-65^{\circ}F$  to
- 1.4 Electrical Equipment
- 1.4.1 A 208 \$10 Volt, three-phase power source at 400 +20 cycles capable of 200 watts with a "CW" and "CCW" switch for the remote trimmers. Switch shall be spring-loaded to "Off."
- 1.4.2 A 0-200 wattmeter with an accuracy of 2% from 100-200-watts.
- 1.5 Symbols Used
- 1.5.1 The following symbols shall be used in this specification:
  - Tf· · · Fuel Temperature ( ${}^{\mathbb{C}}F$ )
  - PLA Power Lever Angle (degrees)
  - Pt2 Compressor Inlet Pressure (psia)
  - Tt2 Compressor Inlet Temperature (°F)
  - Pb Main Burner Pressure (psia) Wf°
  - Metered Fuel Flow (pph) Ratio of fuel in pph to Pb in psia Wf/Pb
  - Throttle Valve Differential Pressure (psi) (Pf2-Pf3) ΔP
  - Nc Control Speed (RPM)
  - Pf2 Control Inlet Pressure (psi)

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1.5.1	(Continued)
	Pfl Control Body Pressure (psi)  Ph Area Control Inlet Pressure (psi)  Po Area Control Drain Pressure (psi)  Pm Area Control Metered Pressure (psi)  Wfm Transducer Valve Fuel Flow (pph)  Pt Transducer Valve Inlet Pressure (psi)  CW Clockwise  CCW Counterclockwise
2.0	Miscellaneous Instructions
2.1	Assemble the control to the drive adapter using two crush washer seals P/N 69397 -26 and -48. Caution should be used to provide correct alignment between control and adapter.
2.2	A calibration of the control shall be completed before running data required by this specification.
2.3	Pfl shall be held within the limits of Curve Number 3 unless otherwise specified. At no time shall Pfl exceed 260 psi.
2.4	Total fuel flow shall be set in accordance with Curve Number 2 unless otherwise specified.
2.5	Whenever CW and CCW adjustments are tabulated in the specification, it is assumed that the adjusting screw is viewed from the head end (drive end) of the screw.
2.6	All log sheets shall contain the rig fuel temperature and specific gravity at the temperature required during calibration.
2.7	The power lever protractor is to be installed on the control and indexed as follows:
	Rotate the power lever clockwise until it hits the stop. While applying 10 inch pounds torque to hold the power lever against the stop, set the protractor to read $0^{\circ}$ .
	Rotate the power lever counterclockwise to second rigging pin hole.
	Install rigging pin (.0920 = .0945 dia.) and protractor must read $67^{\circ} \pm \frac{1}{2}^{\circ}$ .
2.8	All tests are to be conducted with the control connected as defined in Figures 1, 2, and 3.

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2.9 Set all inputs in the increasing direction unless otherwise specified. 2.10 Refer to applicable HS Installation Drawings for control wiring and 2.11 Set the Pb gages to a barometrically compensated manometer before calibrating any section of this specification, depending on Pb. Plot data of paragraphs listed in Appendix M on appropriate curves. 2.12 2.13 Maintain a fuel temperature of 100 ±5°F unless otherwise specified. 3.0 Insepction Requirement The items marked with a single asterisk (\*) in this specification are HSD inspection items and as such must be under 100% inspection by HSD. Only single-asterisked data (\*) shall be transmitted to P&WA. Items marked with a double asterisk (\*\*) shall be inspection witnessed. ₩£L.0 Pre-Hot Test Performance Definition (Section I) 4.1 In order to define the performance of the control after all systems have been calibrated and prior to delivery to the high temperature test rig, the following tests are to be run and data recorded on the rig on which calibration was completed. No adjustments or modifications shall be made after the start of pre-hot-test data recording until the control has completed the high temperature test phase (Paragraph 5.0). 4.2 Proof Pressure CAUTION: DO NOT EXCEED SPECIFIED PRESSURES With PLA at 65°, increase total fuel flow to 20,000 to 30,000 pph and Wf to 10,000 to 15,000 pph. Increase control Pfl to 250 ±10 psi and Pf2 to 料。2。1 1,200 ±20 psi by restricting bypass return flow and control discharge flow respectively. Maintain proof pressures until it is determined that no external leakage exists and leakage from overboard drain does not exceed 50 drops/minute. \*4.2.2 Record external and overboard drain leakage. \*4.2.2.1 Saturate the Tt2 servo to the low temperature stop and set conditions of Appendix B-1. Wf must be within limits of Appendix B-1. Saturate Tt2 servo to high temperature stop and set conditions of Appendix £4.2.2.2 B-2. Wf must be within limits of Appendix B-2. H\*4.3 Minimum Ratio Line

Set: PLA = 15°

Tt2 = 59°

Ne  $\approx 3300 \pm 50 \text{ rpm}$ 

Pt2 = 14.7 psia

Pfl = 100 + 10 psi

Supply Pfl to the min. flow standpipe.

Actuate the remote trimmer to the full CW position.

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4.3	(Conti	nued) Setting Direction	Pf3	W <sub>f</sub> Limits
	10 40 60 100 150 60 40	inc inc inc inc dec dec dec	220+10 220-10 260-20 350-30 450-30 260-20 220-10	1150-1250 1960-2200 2940-3300 4900-5500 7350-8250 2940-3300 1960-2200 1150-1250

#### \*\*4.4 Maximum Ratio Line

Set: PLA = 75° Tt2 = 59°

> Nc = 3553 + 2 rpmPfl = 110 + 10 psi

Pt2 = 14.7 psia

Supply Pfl to the minimum flow standpipe. Vary Pb and Pf3 as tabulated below and record Wf and  $\Delta$  P. Approach each point from indicated direction.

Pb	Setting Direction	Pf3	Item	Limits
15 20 30 70 100 150 125 70	inc inc inc inc inc dec dec	220+10 230+10 280+20 430+30 550+30 725+30 550+30 430+30 230+10	1 2 3 4 5 6 7 8 9	+5 Wf/Fb of Item 5 +4 Wf/Pb of Item 5 +3 Wf/Pb of Item 5 +2 Wf/Pb of Item 5 Record Wf/Pb +2 Wf/Pb of Item 5 +2 Wf/Pb of Item 5 +2 Wf/Pb of Item 5 +4 Wf/Pb of Item 5 +14 Wf/Pb of Item 5

### Compressor Bleed Actuator, Integrating System and Military Droop Bias

Set the conditions of Appendix A of this specification in order, reading from left to right. CBA operation, integrating speed and Wf must be within limits specified.

#### 4.5.1 CBA Instructions

\*4.5

Maintain 40 in. lbs. of torque in the direction to restrain initiation of CBA shaft motion when recording all CBA points. No control of torque is necessary after motion occurs.

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4.5.1 (Continued)

Increase Nc slowly from 2500 rpm until the CBA output shaft rotates fully CCW (bleeds closed). Increase Nc 175 rpm min., then decrease Nc slowly until shaft rotates fully clockwise.

4.5.2 Integration Instructions

Close Valve B and open Valve A shown in Figure 1. Determine the Nc at which integration occurs by increasing Nc slowly and observing transducer metered pressure (Pm). Pm will decrease with increasing speed, but when the integrating piston starts to move, Pm will continue to decrease with no further increase in speed. To determine hysteresis, allow PM to saturate to its lowest level, then decrase Nc slowly until Pm starts to increase; record Nc as hysteresis.

4.5.3 Mil Wf vs Tt2 Instructions

Wf indicated is value obtained at specified Nc set.

\*\*4.6 Remote Trimmer Operation

Set: PLA = 75°

 $Tt2 = 59^{\circ}F$ 

Nc = 3850 + 5 rpm

Pb = 110 psia

Pt2 = 14.7 psia

Pfl = 125 +10 psi

Pf3 = 610 = 30 psi

Actuate the remote trimmer to the CW stop.

- \*\*4.6.1 Record Wf. Wf must be 21230 to 21890 pph.
- \*\*4.6.2 Actuate the remote trimmer to the CCW stop. Record the number of turns which the remote trimmer makes to reach the stop and record Wf at the stop. Wf must be 1980 to 2420 less than the value recorded in 4.6.1.
- Actuate the remote trimmer CW to the stop and record Wf. Wf must be within limits of 4.6.1.
- \*5.0 HIGH TEMPERATURE OPERATION CHECK
- Install the control on a test rig capable of operation with fuel temperatures of 440 ±10°F.

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Set:  $PLA = 70^{\circ} + 5^{\circ}$ 5.1.1

Tt2 = 59+5°F

Nc = 3500 + 50 rpm

Total Flow = 35,000 + 3,000 pph

Pfl = 100+10 psi

Cycle Pb from 30 to 100 Pb three (3) times.

"Plan of Test" JFC-47-1-27 (high temperature fuel test of JFC-47 Production Controls) may be used as a guide only, to fulfill the requirements of this specification.

Set total flows per Curve Number 2.

#### **\*5.2** Minimum Ratio Line

Set: Tf = 100+10 F

PLA= 150

 $Tt2 = 59^{\circ}F$ 

Nc = 3300+50 rpm

Pt2= 14.7 psia

Pfl= 100+10 psi

Supply Pfl to the min. flow standpipe. Actuate the remote trimmer to the full CW position.

Vary Pb and Pf3 as tabulated below and record Wf. Approach each point from indicated direction.

<u>Pb</u>	Setting <u>Direction</u>	Pf3	Wf Limits
10	inc	220+10	1150-1250
40	inc	220+10	1960-2200
60	inc	260 <del>7</del> 20	2940-3300
100	inc	350+30	4900-5500
150	inc	450+30	7350-8250
60	dec	260+20	2940-3300
40	dec	220-10	1960-2200
10	dec	220+10	1150-1250

#### ×5.3 Maximum Ratio Line

Sets Tf = 100+100F

PLA = 75°F+5°

Tt2 = 590 =

Ne = 3553 + 2 rpm

Pt2 = 14.7 psia

Pfl = 110 +10 psi

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5.3 (Continued)

Supply Pfl to the minimum flow standpipe. Vary Pb and Pf3 as tabulated below and record Wf and △ P. Approach each point from indicated direction.

Pb	Setting Direction	Pf3	Item	Limits
15	inc	220+10	1	÷5 Wf/Pb of Item 5
20	inc	230~10	2	44 Wf/Pb of Item 5
30	inc	280+20	3	+3 Wf/Pb of Item 5
70	inc	430₹30	Ц.	+2 Wf/Pb of Item 5
1.00	inc	550+30	5	Record Wf/Pb
1.50	inc	725 <del>7</del> 30	6	+2 Wf/Pb of Item 5
125	dec	550 <del>∓</del> 3 <b>0</b>	7	+2 Wf/Pb of Item 5
70	dec	430+30	8	+2 Wf/Pb of Item 5
20	dec	230+10	9	+4 Wf/Pb of Item 5

\*5.4 Compressor Bleed Actuator, Integrating System, Military Droop Bias

Set: Tf =  $100 + 10^{\circ}$ F. Set the conditions of Appendix A of this specification in order, reading from left to right. CBA operation, integrating speed and Wf must be within limits specified.

\*5.4.1 CBA Instructions

Maintain 40 in. lbs. of torque in the direction to restrain initiation of CBA shaft motion when recording all CBA points. No control of torque is necessary after motion occurs.

Increase Nc slowly from 2500 rpm until the CBA output shaft rotates fully CCW (bleeds closed). Increase Nc 175 rpm maximum, then decrease speed slowly until shaft rotates fully clockwise.

\*5.4.2 Integrating Instructions

Close Valve B and open Valve A shown in Figure 1. Determine the Nc at which integration occurs and hysteresis as explained in Paragraph 4.5.2.

\*5.4.3 Mil Wf vs Tt2 Instructions

Wf indicated is value obtained at specified Nc set.

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5.5 Remote Trimmer Operation
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Set:  $Tf = 440 \pm 10^{\circ} F$ 

 $PLA = 75^{\circ}$ 

Tt2 ≈ 750°F

Nc = 4100 + 50 rpm

Pb = 150 psia

Pt2 = 35 +5 psia

Pfl = 140 + 20 psi

Pf3 = 400 750 psi

#### Operate control at above conditions for 4 hours.

5.5.1 Set:  $Tf = 440 + 10^{\circ}F$ 

 $PLA = 75^{\circ}$ 

 $Tt2 = 59^{\circ}F$ 

Nc = 3500 + 50

Pb = 110 psia

Pt2 = 14.7 psia

Pfl = 125 + 10 psi

Pf3 = 610 + 30 psi

\*5.5.2 Increase No to 3850 + 5 rpm and record Wf.

\*5.5.3 Actuate the remote trimmer to the CCW stop, running the trimmer for 30 seconds "on" and 60 seconds "off" until the stop is reached. This precaution to prevent overheating shall be used whenever the remote trimmer is actuated at elevated temperatures. Record the number of

trimmer is actuated at elevated temperatures. Record the number of turns which the remote trimmer makes to reach the stop and record Wf at the stop. Wf must be 1980 to 2420 less than the value redorded in

Paragraph 5.5.2.

\*5.5.4 Actuate the military trimmer full CW and record Wf. Wf must be within

100 pph of the Wf recorded in Paragraph 5.5.2.

#5.6 High Temperature Comparisons

\*5.6.1 Repeat paragraphs 5.2 through 5.4 with Tf = 440+10°F except that Mil Wf

must be within the tolerance shown in Appendix A for 440°F operation.

\*5.6.2. Repeat paragraphs 5.2 through 5.5.3 with T fuel =  $100 \pm 10^{0}$ F, excluding 5.5.

\*5.6.3 The results of Paragraphs 5.2 through 5.6.2 must agree as follows:

Integrating speeds at 100°F, 440°F and 100°F fuel temperatures must be within specified limits or within +1% of each other.

Remote trimmer check at 440°F must be within specified limits.

Compressor bleed actuator checks at  $100^{\circ}F$ ,  $440^{\circ}F$  and  $100^{\circ}F$  fuel temperatures must be within specified limits.

\*

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5.6.3 (Continued)

Mil Wf vs Tt2 at the two  $100^{\circ}$ F fuel checks shall be within a band width of  $\pm 3$  Wf/Pb. Mil Wf vs Tt2 at  $440^{\circ}$ F shall be within  $\pm 4$  Wf/Pb units and must include the two  $100^{\circ}$ F fuel checks.

If the data is within the limits specified in Appendix A, this shall be acceptable.

\*6.0 FINAL DATA (Section III)

\*6.1 The control shall be installed on a production bench, control adjustments "touched up" as required and final data run. No adjustments are to be made beyond this paragraph.

6.1.1 Set: PLA =  $70^{\circ} \pm 5^{\circ}$ 

 $Tt2 = 59 + 5^{\circ}F$ 

Nc = 3500 + 50 rpm

Total flow = 35,000 + 3,000 pph

Pf1 = 100 +10 psi

Cycle Pb from 30 to 100 Pb three (3) times.

#### 7.0 SUBSYSTEM TESTS

- 7.1 Temperature Servo Calibration
- 7.1.1 Remove AN Plug from end of temperature servo housing for installation of the temperature position indicator (544900 ET-25 Ref.)
- 7.1.2 Index Tt2 Servo Indicator as follows:
  - a. Push Tt2 Piston to end of stroke and measure dimension "B" from indicator mounting surface to Tt2 piston.
  - b. From the assembly check list, obtain dimension "A" from indicator mounting surface to the Tt2 piston, when the follower is in the Pt2 3-D cam detent (850°F).
  - c. Install indicator with Tt2 piston at end of its stroke (a) above and set indicator to read .448 (B-A).

7.1.3 Set: PLA =  $75^{\circ} \pm 5^{\circ}$ 

Pb = 100 psia

 $Nc = 3000 \pm 100 \text{ rpm}$ 

 $Pf3 = 350 + \overline{2}0 psi$ 

Pfl = 85+10 psi

Total flow = 30,000 + 500 pph

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7.1.h With the conditions set in Paragraph 7.1.3, set the Tt2 in the direction indicated and record Tt2 servo dial indicator position.

Tt2	Item	Limits
-65	1	1.120 + .005
0	2	1.026 + .005
59	3	.935 Ŧ .005
300	4	.740 春 .005
550	5	.600 <del>+</del> .005
300	6	+.010 of Item 4
59	7	$\mp$ .010 of Item 3
0	8	+.010 of Item 2
-65	9	→.010 of Item l

- 7.2 No Servo Calibration
- 7.2.1 Remove Cover (P/N 578898 Ref.) and saturation stop screw from top of linkage housing for installation of speed servo position indicator (544900-ET-9 Ref.).
- 7.2.2 Indexing of the speed serve indicator is accomplished as follows:
  - a. Obtain Distance "A" from end of cam push-rod to the cover surface at top of speed servo, when cam is in 1450 rpm L.P. This figure is given on assembly check list.
  - b. Bottom servo in bore by pushing on cam push-rod. Measure from cover surface at top of speed servo to cam push-rod, dimension "B".
  - c. Reinstall saturation screw removed in Paragraph 7.2.1. Set top of screw to a depth of "A" minus screw length, minus 0.142 inches. This will set saturation stop at approximately 200 rpm.
  - d. Install indicator to read servo L.P. and with servo in above position. Set indicator to read (1.357 + A = B).
- 7.2.3 Set: PLA =  $75^{\circ} + 5^{\circ}$ Tt2 =  $59 + \overline{5}^{\circ}$ F Pf3 =  $35\overline{0} + 20$  psi Pb =  $100^{\circ}$  psia Total flow = 30,000 + 500 pph
- 7.2.4 With the conditions set in Paragraph 7.2.3, set Nc and Pfl in the direction indicated and record speed servo dial indicator position.

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7.2.4	(Continued)
10-0-4	/ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~

Ne	Pfl	Item	Limits
1,000	40+5	1	1.432 + .003
1,500	45+5	2	1.348 + .003
2,100	55+5	3	1.201 + .003
2,500	70+10	4	1.085 + .005
3,000	85+10	5	.890 + .005
3,400	100+20	6	.717 + .005
3,800	125+20	7	.521 + .005
4,200	140+25	8	.307 + .006
3,800	125+20	9	+.005 of Item 7
3,400	100+20	10	+.005 of Item 6
3,000	85+10	11	+.005 of Item 5
2,500	70+10	12	005 of Item 4
2,100	55+5	13	+.005 of Item 3
1,500	45+5	14	+.005 of Item 2
1,000	40+5	15	+.005 of Item 1

#### 7.3 Pt2 Servo Calibration

- 7.3.1 Index dial indicator on Pt2 servo as follows:
  - a. Remove cover from Pt2 servo bore.
  - b. Push cam in until it hits stop. Measure distance "B" from Pt2 cover surface to top of the P52 cam shoe. Average 3 readings.
  - c. Assemble dial indicator fixture on Pto cover surface; and, with cam in the above position, set dial indicator to read:

Indicator reading = A-B

Where "A" = dimension from assembly, check list, from Pt2 cover surface to top of cam, when in zero L.P. position.

7.3.2 Set: PLA = 
$$75 \pm 5^{\circ}$$

 $Tt2 = 59 + \overline{5}OF$ 

No =  $3\sqrt{000} + 10 \text{ rpm}$ 

Pb = 100 psia

Pf3 = 350+20 psi

Pfl = 85 + 10 psi

Total flow = 30,000 + 500 pph

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7.3.3 With the conditions set in Paragraph 7.3.2, set Pt2 in the direction indicated and record Pt2 servo dial indicator position.

Pt2	Item	Limits
5	1	.340 ± .006
15	2	.825 ± .006
30	3	1.190 ÷ .006
40	4	1.365 ± .006
30	5	±.015 of Item 3
15	6	÷.015 of Item 2
5	7	÷.015 of Item 1

7.4 Remove dial indicators from Nc, Tt2, and Pt2 servos and install proper covers.

#### \*8.0 PRESSURE CHECKS

\*8.1 Body Pressure, Bypass Flow and Discharge Pressure Sensitivity

Set the conditions shown in Appendix C. Record Wf and  $\triangle P$  for each point and record Wf/Pb where indicated. Wf and Wf/Pb must fall within the limits of Appendix C.

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*8.2 Control Pressure Drop
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Set: PLA = 75° Tt2 = 59°F

Nc = 3850 + 2 rpm

Pb = 184 psia

Record Pf3 and Pf2.

Pf2 - Pf3 must be 85 psi max.

#### \*9.0 MECHANICAL CHECKS

#### \*9.1 Military and Idle Trimmer Range (Manual)

9.1.1 Set: PLA =  $75^{\circ}$  Ff<sub>2</sub> = 14.7 psia Tt2 =  $59^{\circ}$ F Ff<sub>1</sub> = 125 + 10 psi Nc = 3850 + 2 rpm Pf3 = 610 + 30 psi

Pb = 100 psia

Adjust the military trimmer full CCW.

Record Wf. Wf must be 16,600 pph max.

- \*9.1.2 Adjust military trimmer full CW and record Wf. Wf must be 20,500 pph min.
- \*9.1.3 Set the conditions of Paragraph 9.1.1 and adjust the military trimmer to obtain Wf = 19,500 = 19,700 pph.

\*9.1.4 Set: PLA = 15° Pf2 = 14.7 psia
Tt2 = 59°F Pf1 = 55 + 5 psi
Nc = 1980 +2 rpm Pf3 = 200 + 20 psi
Pb = 100 psia

Adjust the idle trimmer full CCW. Record Wf. Wf must be 3,150 pph max.

\*9.1.5 Set: PLA = 15° Pf2 = 14.7 psia
Tt2 = 59°F Pf1 = 55 + 5 psi
Nc = 2280 +2 rpm Pf3 = 200 + 20 psi
Pb = 25 psia

Adjust the idle trimmer full CW.

Record Wf. Wf must be 3195 pph min.

- \*9.1.6 Set the conditions of Paragraph 9.1.4 and adjust the idle trimmer to obtain Wf = 3200 3300 pph.
- \*9.1.7 Set the conditions of Paragraph 9.1.1 and adjust the Military trimmer to obtain Wf = 19,500 19,700 pph.

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	<b>*9.1.</b> 8	Repeat Paragraphs 9.1.6 and 9.1.7 until no further trimmer adjustment is necessary.
	<b>*</b> 9 <b>.</b> 2	Remote Trim Range Check
	*9.2.l	Set the following conditions:
		PLA = 75° +50 Tt2 = 59°F No = 3850 +2 rpm Pb = 110 psi Pt2 = 59°F Pf1 = 125 + 10 psi
	*9.2.2	Actuate the electrical trimmer full CW using the 400 cycle supply. Record Wf and watt meter reading. Wf must be 21,230 - 21,890 pph.
	*9.2.3	Actuate the electrical trimmer full CCW using the 400-cycle supply. Wf must be 1980 to 2420 pph lower than value recorded in Paragraph 9.2.2. Record Wf and wattmeter reading.
:	*9.2.4	Actuate the electrical trimmer full CW using the 400-cycle supply. Wf must be within limits specified in Paragraph 9.2.2.
	*9 <b>.</b> 2 <b>.</b> 5	The watts required by the remote trimmer while increasing Wf and while decreasing Wf shall not exceed 190 watts.
	*9.3.0	POWER LEVER CHECKS
	*9.3.1	Idle Flat Check
	*9.3.1.1	Set: PLA = 13° Pt2 = 14.7 psia Tt2 = 59° Pf3 = 200 + 20 psi Nc = 1980 + 2 rpm Pb = 25 psia Pf1 = 55 + 5 psi Record Wf
	<b>*9.3.1.</b> 2	Set: PLA = 15°  Wf must not change by more than 55 pph from the Wf recorded in 9.3.1.1.
	*9.3.2	40° and 50° PLA Checks

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9.3.2.1 Set: PLA = 50° Tt2 = 59° Nc = 3850 +2 rpm Pb = 100 psia Pt2 = 14.7 psia Pf1 = 125 + 10 psi Pf3 = 470 + 10 psi

Record Wf. Wf must be 14,750 - 15,650 pph.

\*9.3.2.2 Set PLA =  $40^{\circ}$  and record Wf. Wf must be 10,625 - 11,525 pph.

#### \*9.3.3 PL Flat Check

\*9.3.3.1 Set: PLA = 62° Tt2 = 59° Nc = 3850 +2 rpm Pb = 100 psia Pt2 = 14.7 psia Pf1 = 125 + 10 psi Pf3 = 560 + 10 psi

Record Wf. Wf must be 19,300 - 19,900 pph.

\*9.3.3.2 Rotate PLA to 1130 and record Wf. Wf must not vary more than 100 pph during the PLA excursion from 620 to 1130. Record max. variation.

#### \*9.3.4 120° Ramp

\*9.3.4.1 Set PLA = 120° and record Wf. Wf must be 300 - 500 pph greater than the Wf recorded in 9.3.3.2 at 113° PLA.

#### \*9.3.5 PL Hysteresis

\*9.3.5.1 Set: PLA = 1130 and record Wf. Wf must be within +100 pph of the Wf recorded in 9.3.3.2.

\*9.3.5.2 Set: PLA = 62° and record Wf. Wf must be within +100 pph of the Wf recorded in 9.3.3.1.

#### \*9.3.6 PLA Fall-Off Check (60°)

\*9.3.6.1 Set: PLA = 60° and record Wf. Wf must be within 100 pph of the Wf recorded in 9.3.5.2. (62°PLA)

\*9.3.6.2 Set: PLA =  $58^{\circ}$  and record Wf. Wf must decrease 150 pph min. from the Wf recorded in 9.3.6.1 (60° PLA).

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\*9.4.0 SEQUENCING VALVE TEST

9.4.1 Install orifice "W" per Figure 2. Orifice requirements per Paragraph 1.2.15.

9.4.1.1 Set: PLA = 12°

 $Tt2 = 59^{\circ}F$ 

Nc = 2000 + 50 rpm

Pfl = 50 psi

Pf2 = 300 psi (Set with Pb)

\*9.4.2 Recirculating signal pressure shall be 260 psi minimum. S.O.V. signal shall be 125 psi maximum. Record both signal pressures.

\*9.4.3 Note the PLA at which Recirculating Valve Signal is 150 psi. This must occur at 80 to 110 PLA. S.O.V. signal shall be 125 psi maximum. Record both signal pressures.

\*9.4.4 Set PLA to 7°. Recirculating signal and shut-off valve signal must both be less than 125 psi. Record both signal pressures.

\*9.4.5 Note the PLA at which the shut-off valve signal is 150 psi. This must occur at 3° to 6° PLA. Recirculting signal shall be at 125 psi max. Record both signal pressures.

\*9.4.6 Set PLA to 2°. Shut-off valve signal shall be 260 psi minimum.

Recirculating valve signal shall be 125 psi max. Record both signal pressures.

\*9.5.0 POWER LEVER TORQUE TEST

\*9.5.1 Set: PLA = 120°

 $Tt2 = 59^{\circ}$ 

Nc = 3300 + 50 rpm

Pb = 30 psia

Pfl = 100 + 5 psig

Measure torque required to move to 0° PLA and then back to 120° PLA.

\*9.5.2 Power lever torque limits:

From 120° to 65° PLA 5 in-lbs. max. From 65° to 120° PLA 25 in-lbs. max.

From 0° to 65° PLA 25 in-lbs. max. From 65° to 120° PLA 5 in-lbs. max.

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10.0 FUEL FLOW CHECKS

\*10.1 Min. - Max. Line and Min. Flow Check

\*10.1.1 To run a min. ratio line and check min. flow, set:

 $PLA = 15^{\circ}$ 

Tt2 = 59°F

Nc = 3300 + 50 rpm

Pfl = 100 + 5 psi

Supply Pfl to min. flow standpipe to obtain starting min. flow.

Vary Pb and Pf3 as indicated below and record Wf and  $\triangle$  P. Approach each point from indicated direction.

Pb	Setting Direc <b>t</b> ion	Pf3	Wf Limits
-	Charles and the Confidence of the		
10	inc	220+10	1150-1250 pph
20	inc	220+10	1150-1250 pph
40	inc	220+10	1960-2200 pph
60	inc	260+20	2940-3300 pph
100	inc	350730	4900-5500 pph
150	inc	450+30	7350-8250 pph
60	dec	260 720	2940=3300 pph
40	dec	220-10	1960-2200 pph
10	dec	222+10	1150-1250 pph

\*10.1.1.1 Maintain the set conditions of 10.1.1 except increase Pb to 50+5 psia. Set pressure to minimum flow standpipe to 2800 +100 psi to obtain flight min. flow and then reduce Pb to 10 psia and record Wf. Wf must be 1700 to 1800 pph.

\*10.1.2 To run a max. line, set:

 $PLA = 75^{\circ}$ 

Tt2 = 59°F

Nc = 3553 + 2 rpm

Pfl = 110 +5 psi

Supply Pfl to min. flow standpipe. Vary Pb and Pf3 as tabulated below and record Wf and & P. Approach each point from indicated direction.

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10.1.2	Pb	Setting Direction	Pf3	Item	Limits	
	<b>1</b> 5	inc	220+10	1	+5 Wf/Pb of Item 7	
	20	inc	230+10	2	+4 Wf/Pb of Item 7	
	30	inc	280720	3	+3 Wf/Pb of Item 7	
	40	inc	310+30	Ĺ	+3 Wf/Pb of Item 7	
	50	inc	360∓30	5	+2 Wf/Pb of Item 7	
	70	inc	430+30	6	+2 Wf/Pb of Item 7	
	100	inc	550+30	7	Record Wf/Pb	
	125	inc	625 30	8	+2 Wf/Pb of Item 7	
	150	inc	725+30	9	7 Wf/Pb of Item 7	r,
	125	dec	625+30	10	7 Wf/Pb of Item 7	
	70	dec	430 730	11	7 Wf/Pb of Item 7	
	40	dec	310+30	12	+3 Wf/Pb of Item 7	
	20	dec	230+10	13	+4 Wf/Pb of Item 7	

#### \*10.2.0 Starting Schedule

\*10.2.1 Set the conditions shown in Appendix D. Wf must fall within the limits of Appendix D. Record Wf.

#### \*10.3.0 Acceleration Limiting and Topping Schedule

\*10.3.1 Set the conditions shown in Appendix E. Wf must fall within the limits of Appendix E. Record Wf.

#### \*10.4.0 Acceleration Bias, Mil. Wf, Mil Nc, and Topping vs Tto

#### \*10.4.1 Acceleration Bias

\*10.4.1.1 Set the conditions in Appendix F at points coded B and record Wf. Wf must be within the limits specified.

#### \*10.4.2 Mil. Wf

\*10.4.2.1 Set the conditions in Appendix F at points coded F and record Wf. Wf must be within the limits specified.

#### 40.4.3 Mil No

\*10.4.3.1 Set the conditions in Appendix F at points coded S. Determine Nc at which integration occurs as defined in Paragraph 4.5.2 and record. Nc must be within the limits specified. Record Wf at Nc recorded at the start of integration. Record Pm at the start and end of integration.

#### \*10.4.4 Topping

الماره الماره Set the conditions in Appendix F at points coded T. Set Wf with Nc and record Nc. Nc must be within the limits specified.

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MILITARY AND IDLE DROOP LINES \*10.5.0

Set the conditions shown in Appendix G. Wf shall be within the limits speci-\*10.5.1 fied in Appendix G. Record Wf.

IDLE DROOP BIAS \*10.6.0

Set the conditions shown in Appendix H. Wf shall be within the limits speci-\*10.6.l fied in Appendix H. Record Wf.

CDP LIMITER \*10.7.0

Set the following conditions: \*10.7.1

> $PLA = 75^{\circ}$  $Tt2 = 59^{\circ}F$

Nc = 3850 + 2 rpm

Pf1 = 120 + 5 psi

Set Pb to the values listed in Appendix J. Wf shall be within limits of \*10.7.2 Appendix J.

Record Wf and A P.

PROPORTIONAL, CBA AND INTEGRATING SYSTEMS \*11.0

Exhaust Nozzle Area Proportional System \*ll.l

Remove CBA housing. Install a suitable block on top of the integrating piston \*11.1.1 to block the piston .342 in from stop surface on CBA side of bore. Install a dummy CBA cover and bleed the top side of the integrating piston so that the piston will be forced against the block. Install fixed orifices "X" and "Y" as shown in Figure 1. Orifice requirements per Paragraph 1.2.15.

Set:  $PLA = 75^{\circ}$ \*11.1.2

Tt2 = 59°F

Nc =  $3850 \pm 2$  rpm Pb = 100 psia

Pt2 = 14.7 psia

Pfl = 120 + 10 psi

Pf3 = 300 + 50 psi

Ph = 1050 + 10 psi

Po =  $50 + 1\overline{0}$  psi

Close Valve A and open Valve B (Figure 1). NOTE: Set Ft2 and Nc in increasing direction.

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T	
*11.1.3	Vary No in accordance with Appendix K-1. Set Pm = 550 psi using Valve B for each check point and record Wfm. Values must fall within the limits of Appendix K-1.
*11.1.4	Set the conditions of Paragraph 11.1.2, except set: Pt2 = 9.3 psia.
*11.1.5	Vary Nc in accordance with Appendix K-2. Wfm must fall within the limits specified. Record Wfm.
*11.1.6	Set the conditions of Paragraph 11.1.2, except set: Pt2 = 40 psia.
*11.1.7	Vary Nc in accordance with Appendix K-3. Wfm must fall within the limits specified. Record Wfm.
*11.2	Proportional System Deadband
*11.2.1	Set the conditions of Paragraph 11.1.2 with Valve B closed and Valve A open. Set $Nc = 3745 \pm 2$ rpm.
	Approach the above speed in the increasing rpm direction. Note Pm.
*11.2.2	Decrease No until Pm starts to increase above that recorded for increasing No. Speed at this point must be within 40 rpm of speed set in Paragraph 11.2.1. Record No at which Pm starts to increase.
*11.2.3	Increase No to 3940 +2 rpm. Note Pm.
11.2.4	Decrease Nc until Pm starts to increase above that recorded for increasing Nc. Speed at this point must be within 40 rpm of speed set in Paragraph 11.2.3. Record Nc at which Pm starts to increase.
*11.3.0	Compressor Blead Actuator
*11.3.1	Maintain 40 in1bs. of torque in the direction to restrain CBA motion when recording all CBA points.
*11.3.2	Set the conditions shown in Appendix L. Increase the control speed slowly from 2500 rpm until the CBA output shaft rotates full CCW (bleeds close). This speed must fall within limits specified for "Bleeds Close." Record actual speed.
*11.3.3	Continue to increase speed until CBA output shaft rotates full CW (bleeds open or until 4600 rpm is reached. Speed at which bleed shaft rotates must fall within limits specified for "bleeds open," in Appendix L. Record actual rpm.
*11.3.4	Decrease speed to check hysteresis in speeds at which CBA output shaft rotates.

Appendix L.

**\*11.5.3** 

Integrating Speed

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٥٠١١٠
           CBA Filot Valve Actuator Stall Torque and Angular Motion
*11.4.1
           Set: PLA = 15°
                 Pb = 15 psia
                 Nc = 3750 \pm 10 \text{ rpm}
                 Tt2 = 59^{\circ}F
                 Pf3 = 230 psi
                 Pfl = 120 + 5 psi
           Apply 40 in-lbs. CCW to the CBA shaft and set the CBA protractor to zero (0°).
*11.4.2
*11.4.3
           Apply 40 in-1bs. CW to the CBA shaft and record the angle.
           Decrease Nc and record the Nc that the CBA shaft rotated CW.
*11.4.4
*11.4.5
           Apply 40 in-1bs. CCW to the CBA shaft. Record the CBA shaft angle and
           subtract the angle recorded in Paragraph 11.4.3. The difference must be
           greater than 30°.
           Apply 40 in-1bs. CW to the CBA shaft and record the CBA shaft angle.
*11.4.6
           The angle recorded must be less than 35°.
           Decrease speed 20 +2 rpm less than value noted in 11.4.4. Apply CCW torque
*11.4.7
           to CBA shaft. Shaft must not rotate CCW with 75 in-1bs. of torque applied.
           Record torque to rotate shaft if shaft rotates at less than 75 in-lbs.
*11.5.0
           Integrating System & A/B Signal
*11.5.1
           Install orifice "Z" per Figure 3.
*11.5.1.1 Set: PLA = 75°
                 Tt2 = 59°F
                 Pb = 60 \text{ psia}
                 Pt2 = 14.7 psia
                 Pfl = 110 +10 psi
                 Pf3 = 300 psi
                 Ph = 1050 psi
                 Po = 50 +10 psi
           Increase Nc until A/B signal pressure equals 200 \pm 5 psi and record Nc. Nc must equal 3395 to 3535 rpm.
*11.5.1.2
*11.5.2
           Open Valve A and close Valve B (Refer to Figure 1).
*ll.5.2.1 With the conditions set as in Paragraph 11.5.11, determine the speed at which
           the system integrates at increasing speed and at decreasing speed. Record
           speed at each point and hysteresis. Hysteresis shall be less than 20 rpm.
           The speed at which integration occurs is explained in Paragraph 4.5.2.
```

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At end of Int.

With same conditions as in Paragraph 11.5.2.1, record Pm values at which

1000 psi min.

275 psi max.

integration starts and stops. They must be within limits shown.

At start of Int.

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\*12.0 Leakage Checks \*12.1.0 Pb Leakage \*12.1.1 Sets PLA = 75° Tt2 = 59° No = 3850 ±5 Pb = 181 #12.1.2 Soap solution check each joint and seal between the CDP limiter and the control Pb bellows. No evidence of leakage shall occur. Record observations. #12.2.0 External and Overboard Drain Leakage '\*12.2.1 Sets PLA = 65° Tt2 \* 59°F  $Nc = 3710 \pm 5$ Pb = 150 psia. #12.2.2 Using an air hose, remove all traces of fule from the exterior surfaces of the control. Increase Pf3 to 950 ±10 psi and Pf1 to 150 ±10 psi for 5 minutes. There shall be no external leakage and a maximum of 50 drops per minute. \*12.2.3 Overboard Drain Leakage. \*12.2.4 Pressurize overboard drain system to 40 psig for five minutes. External leakage shall not exceed 8 drops/min at each of the following locations: CBA shaft Power Lever shaft Other areas shall have no leakage. The term "no leakage" shall be defined as a permissible visual appearance \*12.2.5 of fluid on the external surface of a control which does not become progressively greater during the prescribed period of time of this test (5 minutes) to such a degree that fluid runs off the surface of the control or forms droplets. \*13.0 Audit Test \*13.1 Lockwire Control as required. \*13.2 At the following audit set points record as required.

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\*13.2.1 Minimum Ratio Line Check

Sets PLA = 15°

Tt2 = 59°F

 $Ne = 3300 \pm 2 \text{ rpm}$ 

Pfl = 100 ±5 psi

Record Wf at Pb = 40 psia, Pb = 150 psia and hysteresis at Pb = 40 psia. (Ref. Par. 10.1.1

\*13.2.2 Maximum Ratio Line Check - Set: PLA = 75°

Ne = 3553 rpm

Tt2 = 59°F

 $Pf1 = 100 \pm 5 psi.$ 

Record Wf at Pb = 20 psia, Pb = 150 psia (Ref. Par. 10.1.2).

\$13.2.3 Starting Accel. Limiting and Mil Droop - Set the following conditions and record Wf as required: (Para 10.2.1, 10.3.2 and 10.5.1.)

Tt2	PLA *	Pb	P <b>f</b> 3	Pfl	Ne	Wf
59 <b>°</b> 59 <b>°</b>	75°	15.5	240	40	815	Record
59° 59°	75°	40 100	315 525	60 100	2214 32 <b>62</b>	
59°	75°	110	595	120	3850 ,	

\*13.2.4 Idle Droop - Set the following conditions:

PLA = 15°

 $Ne = 1980 \pm 2$ 

Tt2 = 59°

Pfl = 55 psi.

Pb = 25 psis.

Record Wf. Increase speed to Nc = 20 $\pm$ 10 then dec. to Nc = 1980 ±2 and record Wf as Idle Droop Hysteresis (Ref. Para 10.6.1).

\*13.2.5 Military Droop Bias - Set the conditions marked (A) in Appendix F Record Wf. (Ref. Para 10.4)

\*13.2.6 Integrating System - Set the following conditions and record at speed which integration takes place (Ref. Para 4.5.2)

PLA	Pb	Tt2	Pt2	Ne
75°	60	59°	14.7	
75°	60	300°	14.7	

\*13.2.7 Compressor Bleed Actuator

Set the following conditions: PLA = 75°

Tt2 = 59°F

Pb = 50 psia

Increase speed until the CBA output shaft rotates fully in the CCW direction. Record Nc at which motion occurs. (Ref. Para. 11.3.0)

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\*14.0

#### Preservation and Storage

At the conclusion of performance testing, drain the calibration fluid from the control and prepare the control for shipment in accordance with HS Specification 380.

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			M.	₩-	and the first supple					- 7	-K

\*Set Pfl to 60 psi or lower before setting this value.

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# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT, U. S. A.

			`	Tt2 FAILSAFE	CHECK	j.
				(Para. 4.2.2) Appendix B-1		
,			LOW	Temperature	Fellsafe	
Connect	Pfl to	Min. Flow	w Standpipe			
PI'A	9 l Z	Ä		6. 3. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	(Reference) Ratio Units	W.T.
ກັກກ	1048 1514 1980	222	SAN.	4 H M	76.96 121.65 173.26	1419 - 1659 2313 - 2553 6690 - 7170
វីបវិបុរីប	2505 3029 3195	တ္မွ ဥ ဥ	5 6 5 F.	388 700 730 73	176,77	9 0 8
i jir	1019	100	) M M	なった。	127.07	0
			High	Appendix B	-2 Failsafe	
Connect	Pfl to	Min. Flow	Stand			
<i>ክ</i> ኯኯ	1048 1514 1980	20 20 10	がだり がなる	175 175 305	76.87 121.65 173.26	1417 - 1657 2313 - 2553 6690 - 7170
だだがが	2505 3029 3495 4019	100	10.000 135.50	385 700 175 175	*176,77 = 176,93 *145,15 = 139,96 *130. = 123,89 127,07	0 0 0 0
* These	yalues	reflect	minimum and	and maximum cam	rotation due to tolerance	

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		ВС	DDY PRE	essure, i	the state of the s	PPENDIX C Para. 8.0 LOW AND BACK PR	ESSURE S	E&SITIVITY	
1	PLA Deg.	Tt2	N <sub>C</sub>	Pb psia	Pfl psi	Total Flow PPH	Pf3 psi	Wf PPH	
	Body I	Pressur	e Sees	itivity					
-	75°	59	3800	20	170	38,000±500 38,000±500	290	Within 60 pph Recor	·d
2. 3.	75° 75°	59 59	3800 3800	20 20	135 90	38,000±500 38,000±500	255 210	Record Recor Within 70 pph Recor	
4.	75°	59	3800	100	270	38,000±500	460	of item 2 Within 100 Recor	·d
5. 6.	75° 75°	59 59	3800 3800	100 100	135 90	38,000±500 38,000±500	425 380	Record Record Within 100 Record of item 5	
	Bypass	Flow	Sensit	ivity (F	ligh Alti	tude Effect)			
1.	75° 75°	59 59	3800 3800	20 20	120 120	10,000±500 20,000±500	225 225	Record Record Within 30pph Record	
3.	75"	59	3800	20	120	30,000±500	225	of item 1 Withir 60 pph Recor of item 1	·đ
Ц.	75°	59	3800	20	120	40,000±500	225	Within 90 pph Recor	·d
5. 6.	75°	59 59	3800 3800	50 50	120 120	15,000 <b>±5</b> 00 20,000 <b>±5</b> 00	35C \$	Record Recor Within 50 pph Recor	
7.	75*	59	3800	50	1.20	30,000 <b>±500</b>	35C - S	of item 5 Within 60 pph Recor	·đ
8.	75°	59	3800	50	1.20	40,000±500	35C	of item 5 Within 90 pph Recor of item 5	ď
,						esecutive Wf/Pb	values :	recorded at points l	
		re: eur	e Sens	itivity	•				
1. 2., 3.	75° 75°	59 59 59	3800 3800 3800	100 100 100	120 CLI 120	38,000 38,000 38,000	800 600 1400	Record Within 150 pph of item Within 250 pph of item	

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#### APPENDIX D

Para. 10.2.0

#### STARTING SCHEDULE

PLA (deg)	Tt2	Pb (psia)	Pf3 (psi)	Pfl (psi)	$\frac{Nc}{(rpm)}$	Ratio Units (ref)	( <del>Wf</del> (pph)
15	59°	15.5	170	40	815	61.4	1150 - 1250
15	59°	16.5	170	40	990	72.4	1150 - 1290
15	59°	18.0	180	40	1165	87.0	1530 - 1675
15	59°	19.5	195	40	1398	111.0	2125 - 2280
15	59°	20.5	205	45	1515	121.7	2455 - 2620
15	59°	22.0	210	45	1631	130.8	2830 - 3010

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#### APPENDIX E

Para. 10.3.0

#### ACCELERATION AND TOPPING SCHEDULE

ar a							
Tt2 (°F)	PLA (deg)	( <u>Pb</u> (psia)	Pfl (psi)	Pf3 (psi)	$\frac{Nc}{(rpm)}$	$\frac{\text{Ratio}}{\text{Units}}$	<u>wr</u> (pph)
59°	75°	20	40	170	990	72.4	1330 - 1570
59°	75°	20	40	180	1165	87.1	1620 - 1860
59"	75°	20	45	210	1515	121.7	2315 - 2555
59*	75°	25	50	260	1864	160.7	3870 - 4170
59°	75°	40	60	320	2214	181.0	7000 - 7480
59°	75°	60	75	400	2680	186.8	10850 - 11570
59°	75°	100	90	540	3029	172.0	16600 - 17800
59°	75°	100	95	510	3262	158.0	15200 - 16400
59"	75°	100	110	575	3553	178.3	17230 - 18430
59°	75°	110	150	575	4311-4427	169	18600
59°	75°	120	150	550	4369-4485	140	16800
59°	75°	160	40	700	<b>O</b> *	.161	24100 - 26700

<sup>\*</sup> Sat Wf Total = 40,000 #2000 pph for this point only.

# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT, U. S. A.

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								٠.,										,
		Limits		3791 - 3908	-	·	4022 - 41144	j Ja	4022 - 41144			3944 - 4022		3853 - 3932	:		3845 - 3920	4252 - 4369
F and Topping vs. Tt2		Wf Int. Limits No 8715 - 9315	21230 - 21890		7100 - 7515	24950 - 25800		16706 - 17276		13462 - 13962	11516 - 11942		13698 - 14,238		1090 - 1390	8160 - 8520		
APPENDIX F. Mil No, and To Para, 10,4)	t	Kecord							i	, ·								5700
APPEI Wf, Mil (Para		Pf3 370	610	019	325	069	069	525	525	760	730	430	7.0	170	260	360	360	310
Blas, Mil Wf		Pf1 85	120	120	85	170	170	071	077	130	130	130	120	120	85	120	120	150
Accel, B		Pt2 14.7	14.7	14.7	21.7	21.7	21.7	13	13	15	15	15	21.7	21.7	18	18	18	18
Ace		Pb 50	110	110	35	142	242	56	95	83	71	7.1	8	06	25	.09	09	50
න : ගු	Speed	Nc 2913	3850		2913	4083		4083		3981	3981		3893		2913	3882		\$- <sub>1</sub> 4 }
۰H	Mil Wf Mil Set Topping	Tt2	59°	26	150	150	150	150	150	300A	300	300	415	514	550	550	550	550
<u>1</u>	0 0 0	Code	[iz.	တ	ф	í <del>t</del> i	ഗ	Íz.	တ	달 ,	, <b>5</b> 4	ω, ,	Ē	တ	щ	ᄄ	ß	₽

# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT, U. S. A.

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														· ·					A <sup>A</sup>	****	
	Nc Limits 4311- 4427			3824 - 3900		3824 - 3900		3852 - 3932	•		38७७ - १०५५		4022 – לעונין		3791 - 3908	•		·	3585 - 3696		3791 - 3908
	Into															1 49					
Ç	Limits	2860 - 3100	3300 - 3470		2121 - 2229		2237 - 2326		4055 - 4205	2920 -3028		3517 - 3637		3860 - 3980		9110 - 9950	8875 - 9595	7832 - 8096		9650 - 9950	•
APPENDIX F (cont.)	ME WE					•															
APPEND	Pf3 265	220	240	240	240	240	250	250	250	250	250	260	260	240	240	390	380	320	320	375	375
	Pf1 150	85	120	120	120	120	130	130	130	130	130	170	140	120	120	85	85	110	110	120	120
	Pt2 18		12						3.1	3,1	٣. د	2.4	2.4	2.3	2,3	2,3	2,3	2,3	2,3	7.2	7.5
	Pb 50	20	28	28	18	18	14.7	14.7	23	18	18	20	50	50	50	20	09	7/1	717	20	50
	No	2913	3862		3862		3893		3981	3981		4083		3850		2913	.2913	3623		3850	
	Tt2 550	750	750	750	750	750	415	415	300	300	300	150	150	59	59	65		<b>V</b> O		5,9	59
	Code	Д	ĒΨ	മ	[īz.,	മ	ഥ	ഗ	[354	<b>[54</b>	മ	ᄕᅺ	<b>്ര</b> ,	Ē.	ഗ	В	Ф	. <del>[2</del> 4	ഗ	ᅜ	<b>S</b> 3

# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT, U. S. A.

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#### APPENDIX G

Para. 10.5.0

#### MILITARY AND IDLE DROOPS

	PLA	Mi. O	#ma				
	$(\frac{r_{11A}}{\text{deg}})$	Tt2 (*F)	Pb (psia)	Pfl(F		Direction of Approaching	$\frac{\text{of}}{\text{Nc}}$ $\frac{\text{Wf}}{(\text{pph})}$
	APPEwD IDLE D	IX H ROOP					
10	15	59	25	55	1922±2	Increase	610-930 more that item 2
2.	15	59	25	55	1980±2	Increase	3150-3350
3. 4.	15 Increas	59 se No <b>to</b> 380	25 00 rpm	55	2039±2	Increase	705-1025 less than item 2
5.	15	59	25	55	1980±2	Decrease	Within ±205 of item 2
6.	15	59	25	55	1922±2	Decrease	Within ±205 of item 1
	MILITAR	Y DROOP			# n.		
F-4-0	75	59	110	120	3740±2	Increase	295-510 more than item 3
2.	75	59	110	120	3790±2	Increase	155-270 more than item 3
3.	75	59	110	120	3850±2	Increase	21230-21890
	75	59	110	120	3900±2	Increase	145-250 less than item 3
5.	75	59	110	120	3940±2	Increase	240-415 less than item 3
5.	75	59	110	120	3850±2	Decrease	Within ±215 of item 3

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APPENDIX H

Idle Wf versus Tt2

(Para. 10.6)

						and the second s
PLA.	Tt2	No.	Pb	Pfl_	Pf3	Limits of Wf
<b>1</b> 5	-65	1980	25	55	205	2,630 - 2,830
15	0	1980	25	55	205	2,915 - 3,115
15	59	1980	25	55	205	3,150 - 3,350
15	150	1980	25	55	205	2,535 - 2,735
15	250	1980	25	55	205	3,310 - 3,510

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APPENDIX J
(Para. 10.7.0)
CDP LIMITING

Pb	Direction of	PPH	PPH			
psia	Approaching Pb	<u>Min</u>	Max			
184	Inc.	35,500	36,600			
186	Inc.	31,300	36,800			
188	Inc.	23,100	36,800			
192	Inc.	12,000	19,900			
186	Dec.	31,300	36,800			
184	Dec.	35,500	36,600			

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## APPENDIX K Para. 11.2 AREA PROPORTIONAL SYSTEM SLOPE

Appendix K-l	
No RPM	Wfm Limits (pph)
3670	319 to 433 less than Wfm recorded at
3790	Record
3850	Record
3905	Record
4020	334 to 454 more than Wfm recorded at 3850 Nc
Appendix K-2	•
3745	319 to 433 less than Wfm recorded at 3850 Nc
3850	Record
3945	334 to 454 more than Wfm recorded at 3850 No
Appendix K-3	<b>~</b>
3540	319 to 433 less than Wfm recorded at 3850 Nc
3850	Record
4150	334 to 454 more than Wfm recorded at 3850 Nc

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	Hysteresis for Bleeds Close		28 to 72 rpm	from close rpm 28 to 72 rpm	from close rpm 28 to 148 rpm from	close rpm 28 to 100 rpm from	slose rpm. 28 to 100 rpm from
d Schedule	Hysteresis for Bleeds Open	Charles to the section of the sectio	28 to 72 rpm	from open rpm 28 to 72 rpm	from open rpm		
Compressor Bleed Schedule	Limit of Nc for Bleeds Open	AND THE PROPERTY OF THE PROPER	3961 max.	4296 мах。			
APPENDIX L ef. Paragraph 11.3 )	Limits of Nc "Bleeds Close"		2877 - 2936	3274 - 3338	3833 - 3909	4179 - 4261	
(Re	T+2	CT (This was a few to a	−65° F	59° F	150° F	250° F	i j
	q <sub>d</sub> .	CHARTELLY 1	50	20	50	50	િલ્ -
	PLA	CHESTONIC	65	65	65	65	

# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT, U. S. A.

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#### APPENDIX M

	Appendix and a management of the control of the con	
Curve Number	Name	Applicable Para.
F-5690	Proportional Gain	11.1, 11.2
F-5691	Tt2 Failsafe	4.2.2
F-5692	Min Ratio, Min Flow	4.3, 5.2, 5.6.1 5.6.2, 10.1.1
F-5693	Max Ratio	4.4, 5.3, 5.6.1 5.6.2, 10.1.1
F-5694	Starting Accel and Topping	10.2, 10.3
F-5695	Accel Bias	10.4
F-5696	Pressure Sensitivity	8.0
F-5697	Power Lever	9.3
F-5698	Sequencing Valve	9.4
F-5099	Idle and Military Droop, Idle Bias	10.5, 10.6
F-5700	Military Droop Bias	4.5.3, 5.4.3, 5.6.1, 5.6.2, 10.6, 10.4
F-5701	Integrating Speed	4.5.2, 5.4.2, 5.6.1 5.6.2, 10.4
F-5702	Compressor Bleed Actuator	4.5, 4.5.1, 5.4.1, 11.3, 11.4
F-5703	CDP Limiter	10.7
	Non-Plottable	
,	Remote Trimmer	4.2.1
	Trimmer Range	4.6 5.5
	Proof Pressure	9.1 9.2
	P.L. Torque	9.5 12.0
	Max Control Pressure Drop	
	Leakage	· ·

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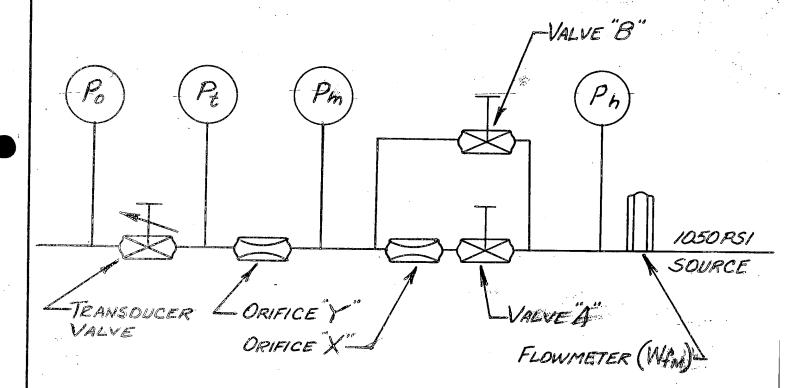
PAGE \_\_\_\_OF \_\_

FIGURE 1

INTEGRATION

PROPORTIONAL GAIN

(PARA. 11.1, 10.4)



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WINDSOR LOCKS, CONNECT	ICUT . USA

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PACE 42	

FIGURE 2 SEQUENCING VALVE (PARA. 9.4)

RECIRCULATING SIGNAL
GAGE

SHUT-OFF SIGNAL
GAGE

ORIFICE'W"

RECIRCULATING VALVE SIGNAL

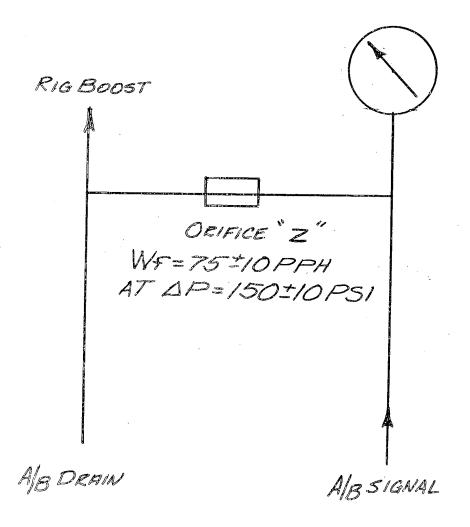
SHUT-OFF VALVE SIGNAL HS F-755. 18 6/62

## Hamilton Standard DIVISION OF UNITED WINDSOR LOCKS, CONNECTICUT . U.S.A.

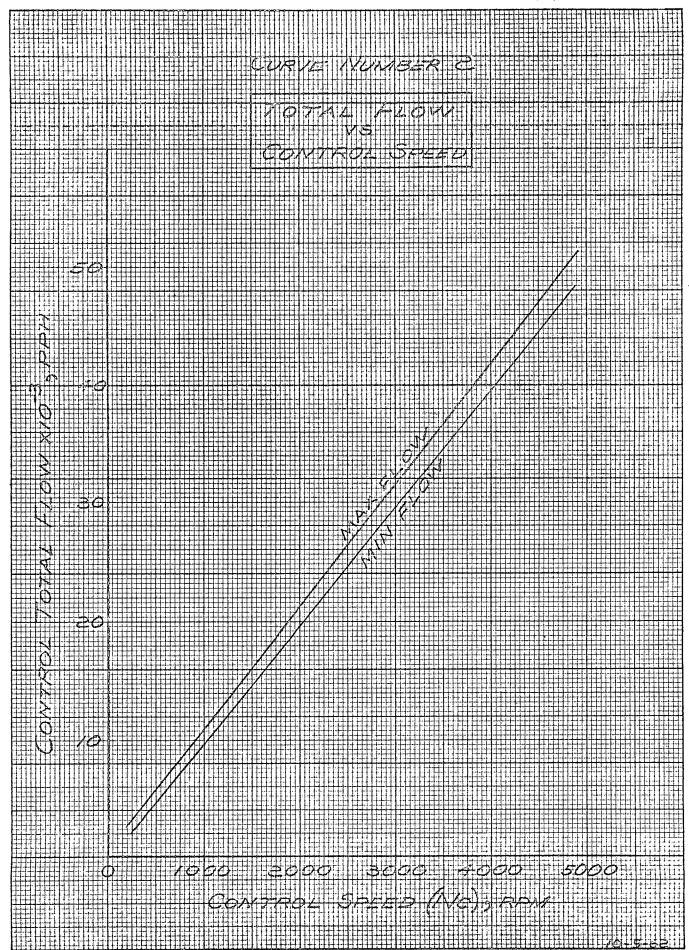


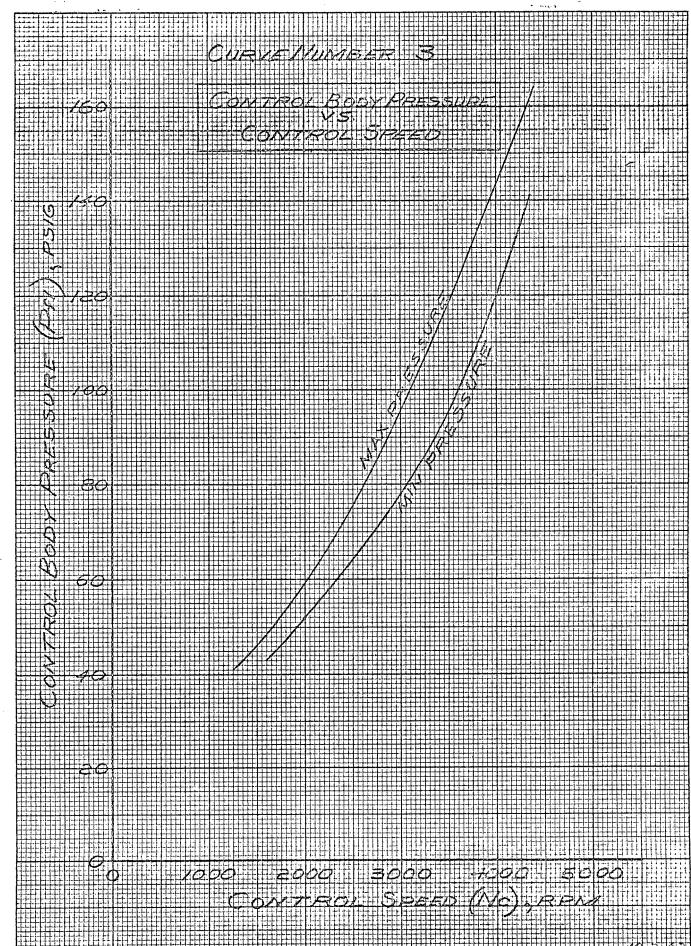
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FIGURE 3 A/B SIGNAL (PARA 11.5.1)



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1	WENVERNER FOR MARCHE STATE STA	
	FOUNTESS CONTROLESS AND ESTANDED POSS SON	5 30 35
	ARE PRESSURE (VI)	15 20 2 W\\\\\\\\\\\
	COMPRESSOR DISCLAR	
	2	0







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## HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION

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WINDSOR LOCKS, CONNECTICUT, U. S. A.

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1.0 GENERAL INFORMATION

1.1 Annulments

This specification supercedes all previous qualifications and/or letters of instruction covering these assemblies.

- 1.2 <u>Scope</u>
- 1.2.1 Where noted on the assembly drawing, this specification defines the methods of calibrating and testing for acceptability of applicable JFC-47 Linkage Components furnished as spares or assembled into Fuel Controls at HSD.
- 1.3 Test Requirements
- 1.3.1. 'Unless otherwise specified, all pressures are gage.
- This specification defines a test procedure for determining the position of the Pb Input Lever which will produce the minimum pressure effect from the sealing bellows. The procedure defined in Para. 2.4 thru 2.5.2 is a suggested procedure for determining this point. The test in Para. 2.5.3 proves that minimum pressure sensitivity point has been found.

  The calculation of net weight -w- at the minimum pressure sensitivity position is necessary to insure that the torque imposed by the bellows and flexure springs does not exceed the range of the fuel control adjustments.

The pivot contact test is required to insure that the lever pivots are seated at the minimum operating load when the lever is in the minimum pressure sensitivity position.

- 1.4 Equipment Required
- 1.4.3. Tooks which parmit proper assembly of components and plumbing of test fixtures.
- 1.4.2 Nacessary fixture as described in Appendices.
- Letes Presumatic pressure source capable of maintaining for a minimum period of 1/2 hour any set pressure, within 22 pai, between 0 and 200 pai.
- Lahah Pressure gages e One gages 0-200 psis & 2.5% accuracy.
- la4.5 Measuring gages → One 12 inch height gage, .0001 accuracy.
- 1.4.5 Dial indicators = One 1 inch stroke, .0001 accuracy.

#### HAMILTON STANDARD

SPEC. NO. HS 1558B

### DIVISION OF UNITED AIRCRAFT CORPORATION

CODE IDENT NO. 73030

WINDSOR LOCKS, CONNECTICUT, U. S. A.

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- 1.4.7 Set of weights, one quarter (1) lb. subdivisions, four (4) lb. total.

  Weights are to be accurate within 1%.
- 1.4.8 One 25 lb. soule, accurate to one ounce.
- 1.4.9 Set of weights, one cunce subdivisions, one quarter  $(\frac{1}{4})$  lb. total, weights are to be accurate within 1%.
- 2.0 P3 Lever Assembly (Reference Appendix A schematic).
- 2.1 Measure and record dimension e to nearest .005 inch. Dimension c will, equal 1.233 + .004 from detail drawings. Determine dimension d from the equation d = e 1.233. Calculate and record dimension.d.
- 2.1.L Weigh and record actual weight of 10:0.5 lb. weight plus its lever attachment fixtures. Secure the lever attachment fixture at point E.
- 2.2 Mount P3 lever assembly onto .094 DIA dowel pins and secure the lever assembly to the fixture.
- . 2.3 Attach a 10 k 0.5 weight at point E, adjusting the weight stop such that the 10 lb. weight is just beginning to act on the lever.
- 2.3.1 Attach the dial indicator with its probe on the .093 dia, pin. at point B.
- 2.3.2 Attach the weigh pan on the .093 dia, pin. Back off the weight stop approximately .100 inch. Add weight to weigh pan such that a parallel or "null" condition is reached (i.e. dimension a equals dimension b within .0005 inch).
- 2.3.3 Record total "mull" weight (this weight includes everything attached to point B).
- 2.3.4 Zero the dial indicator at "null".
- 2.4 Install scaling cover and set Pd 50 psi.
- 2.4.1 Add 2 lb. weight to the "null" weight. Record displacement of point B.

  Decrease weight by 4 lb. in \$\frac{1}{2}\$ lb. increments, recording displacement of point B at each set point.
- 2.4.2 Set Pd = 0. Add 2 lb. to establish "null". Hand adjustment of weigh pan may be necessary to obtain the null point. This hand adjustment will remove any residual friction forces in the pivota.
- delia? Repeat Pouch at Pd = 100 paid
- 2.h.h Reput 2.4.2
- 2.4.5 Repeat Cohol at Fd a 150 pais

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### HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION

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- 2.4.6 Rebeat 2.4.2
- Plat W (weight ended and subtracted from "null" weight) wersus X (displacement of point B) for Pd = 50, 200, 150 psi. Connect the points common to each pressure with a straight line. See Appendix B for an example plot.
- Determine position X corresponding to the intersection of the three plotted lines, or the average X corresponding to the minimum band width of the intersection of the fames plotted lines. This is the point of minimum body pressure (Pd) sensitivity of the Rever assembly and establishes the steady state attitude which the Ph lever dust assume in the control. Also determine the total weight at point B which a responds to position X. Record this weight.
- 2.5.2 If the X determined in 2.5.1 and used in 2.5.3 is greater than 4.012 inch, the lever assembly is unalleptable.
- 2.5.3 Verify this middle body pressure sensitivity point as follows. At Pd = 50 psi add 2 lb. weight. Decrease weight until the dial indicator reads the X determined in 2.5.1. Increase Pd to 150 psi recording X at 50, 100, 150 psi. X must not change by more than .0005 inch. If X changes by more than .0005 inch, the lever assembly is unamorphable. Tap fixture lightly during this test to remove pivot friction effects.
- 2.6 Remove the PB lever assembly. Vibrator engrave the I determined in 2.5.1 on the proper surface of the lever in this manners x = pos. or neg. X determined in 2.5.1. Example, X = neg. .008. Vibrator engrave the net aeight F determined in 2.7.2 on the proper surface of the lever in this manners F = pos. or neg. F: Example, F = pos. .75 lb. This information will be area to install the PB lever assembly into the Control per HS specimation of ablos .500 sich that one lever will be non-sensitive to body pressure.
- 2.6.1 Report data taken in 7.5.5; sectal number of assembly (if applicable), the sector of assembly.
- 2.7 Westermies the net force sequired at point B to obtain position X as follows.
- 1.7.4 Ministry the wedget (posside) remorded in 2.1.1 by dimension d (inches). Distinct consists by dimension g (inches).
- R.7.2 Fire the difference had wear the final result in 2.7.1 and the total weight recorded in Para. This difference F must not exceed 2 pounds. Record this set delegate Fe. Not weight in positive if setual weight recorded in Para.
- 7.7.3 It has whicht on obtained in 2.7.7 To greater than 2 pounds, the P3 lever
- 9.8 Declaration that learn park to are in about set with lever in optimum operating position and follower
- 2.8. Install less foto fortuna as about in Appendix C.

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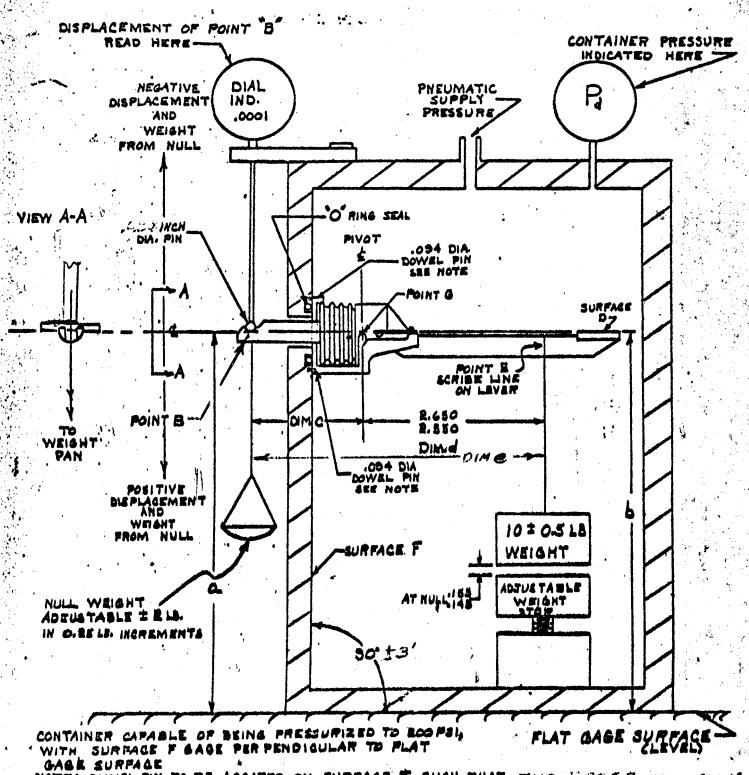
2.8.2	Apply 6.0 ± 0.10# weight at point *H* on leading spring.	ever to simulate pivot contact
2.8.3	Apply 1.1 + 0.10# weight at point E en leve	er.
2.8.4	Adjust micrometer to move lever until dim002 inch. Record micrometer reading.	Ran equals dim. "b" within
2.8.5	Adjust micrometer to move lever to the *X* paragraph 2.5.1. This may be done by adjust amount scribed on the lever as dimension *I must be in contact with .100 dia. pin at the	sting the micrometer by the
2.8.6	With the lever in this position there must either of the pivots for the lever (point exceeds .001 lever is unacceptable.	be no more than .001 gap at "G"). If gap at either pivet
3.0	P3 Lever Assembly 576053	
3.1	Test 576053 for acceptability per 2.0.	
4.0	P3 Lever Assembly 576096	
4.1	Test 576096 for acceptability per 2.0.	
5.0	P3 Lever Assembly	· · · · · · · · · · · · · · · · · · ·
5.1	Tost 581610 for accentabilities man d o	

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### APPENDIX A

### JFC-47 LINKAGE COMPONENT CALIBRATION P. LEVER ASSEMBLY



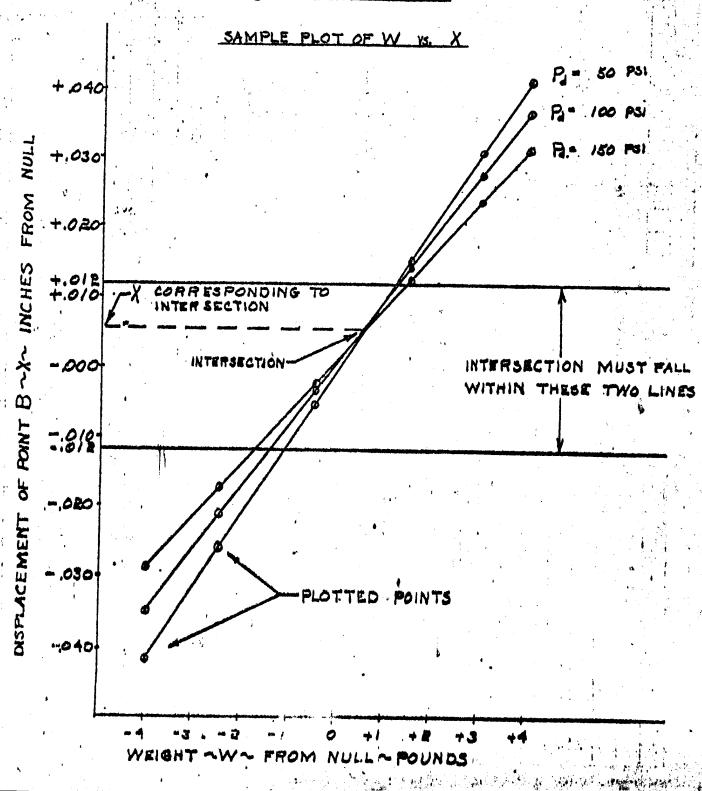
NOTEL DOWAL PIN TO BE LOCATED ON SURFACE F SUCH THAT THE WIPPER DOWIEL-13

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### APPENDIX B

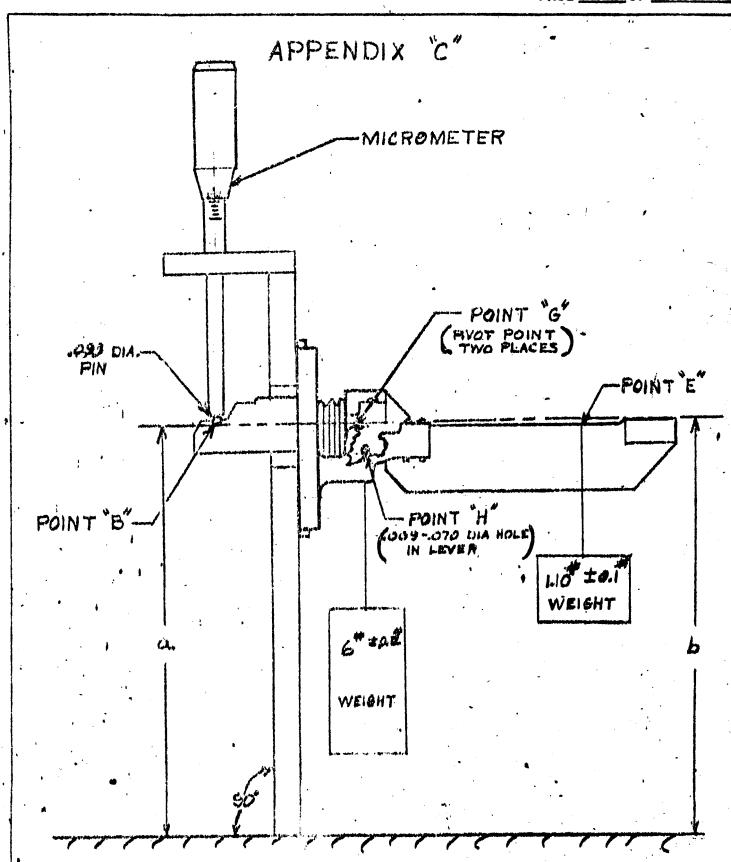
TFC-47 LINKAGE COMPONENT CALIBRATION
B LEVER ASSEMBLY



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TEST SET-UP TO GRECK FOR PIVOT CONTACT RER PARA 2.9

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Amendment	2
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Change paragraph 2.6 to read:

"Remove the P3 lever assembly. Vibrator engrave the X determined in 2.5.1 on the proper surface of the lever in this manners X = pos. or neg. X determined in 2.5.1. Example, X = neg. .008. Vibrator engrave the weight -w- corresponding to the X determined in 2.5.1 on the proper surface of the lever in this manners w = pos. or neg. w corresponding to X determined in 2.5.1. Example, w = pos. 0.75 lb. This information will be used to install the P3 lever assembly into the Control per HS specification 1502 such that the lever will be non-sensitive to body pressure."



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CODE IDENT NO. 73030

1.0	GENERAL INFORMATION
1.1	SCOPE
1.1.1	This specification covers the method of calibrating and testing the JFC-47 Tt2 sensor for temperature compensation.
1.2	Equipment Required
1.2.1	A nitrogen pressure source and regulator of 20 psig.
1.2.2	A nitrogen pressure source and regulator of 250 psig.
1.2.3	One mercury U tube manometer capable of ±25" HG.
1.2.4	One pressure gage with a range of 0-50 psi and an accuracy of 1%.
1.2.6	Fixtures: 569455-T-17 569455-T-154
1.2.7	One oven capable of 500°F and large enough to contain the JFC-47 temperature cover and associated fixtures required for conducting this test. Provisions should be made for tapping the Tt2 cover assembly from outside the oven.
1.2.8	Force indicator with a range of 0 to 5.0#.
1.3.0	Symbols
1.3.1	The following symbols will be used throughout this specification:
	Ps = Simulator Pressure (psig) Pns = Null Sensor Inlet Pressure (psig) Pml = Null Sensor Metered Pressure (in Hg) Pm2 = Null Sensor Metered Pressure (in Hg)
1.4	Test Requirements
1.4.1	The control component shall have been assembled and dry calibrated in accordance with HS 1502B and HS1503A.
2.0	Set up and Testing of Temperature Sensor
2.1	Set-up of Fixture 569455-T-154

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Connect the null sensor inlet pressure source (20 psig) to the null sensor assembly. (Fixture should not be mounted onto the Tt2 cover at this time.) Connect the Pml and Pm2 lines to the manometer and apply 20 psig to the null sensor assembly. Using the force meter, apply a 2.5# force at the Pilot Valve pin and adjust set screw A until Pml = Pm2. See Figures 1 and 2.

- 2.1.2 Loosen null sensor mounting screws B and C and install Fixture 569455-T-154 onto the Tt2 cover. Install the .501 gage block of fixture 569455-T-17 between the multiplying lever and input lever, and adjustathe null sensor against the multiplying lever until Pml = Pm2. Lock screws B and C.
- Install Tt2 feedback rollers onto Fixture 569455-I-154 and mount fixture onto Tt2 Cover. See Figure 1. Align pushrod and micrometer head assembly so that rollers and pushrod are parallel to and midway between the multiplying and input levers.
- 2.1.4 Turn and micrometer head in until the Tt2 feedback rollers contact the Tt2 multiplying lever pivot bracket. Loosen Set Screw D and adjust micrometer head to read .355%.
- 2.2 Calibration Check of Tt2 System
- Set micrometer at 1.10" and adjust Ps until the mercury manometer is at zero  $\Delta P$  and record Ps. Using this technique, run the entire calibration schedule per Appendix A at Room Temperature. Tap the Tt2 cover and fixture assembly while taking reading. A preliminary run should be made prior to taking data, to properly seat the moving parts.
- After completing the schedule per Para 2.2.1, review the data to determine the hysteresis at each roller position. If it is in excess of 1.5 psi over the entire range, it is caused by misalignment of the roller assembly. If this is the case, realign the roller assembly and rerun the schedule per Para 2.2.1. If hysteresis is in excess of 1.5 psi for only one or two roller positions, disregard these points and continue with testing.
- Having satisfied the requirements of Paragraphs 2.2.1 and 2.2.2, increase the temp. to a value that is 355°F ±5°F above room temperature. Allow temperature to stabilize for 30 minutes and repeat Para 2.2.1 and 2.2.2 if necessary at this temperature.
- 2.2.4 Reduce temperature to room temperature and return the unit to the assembly area, together with the data, for evaluation.
- 2.3 Assembly Area Instructions

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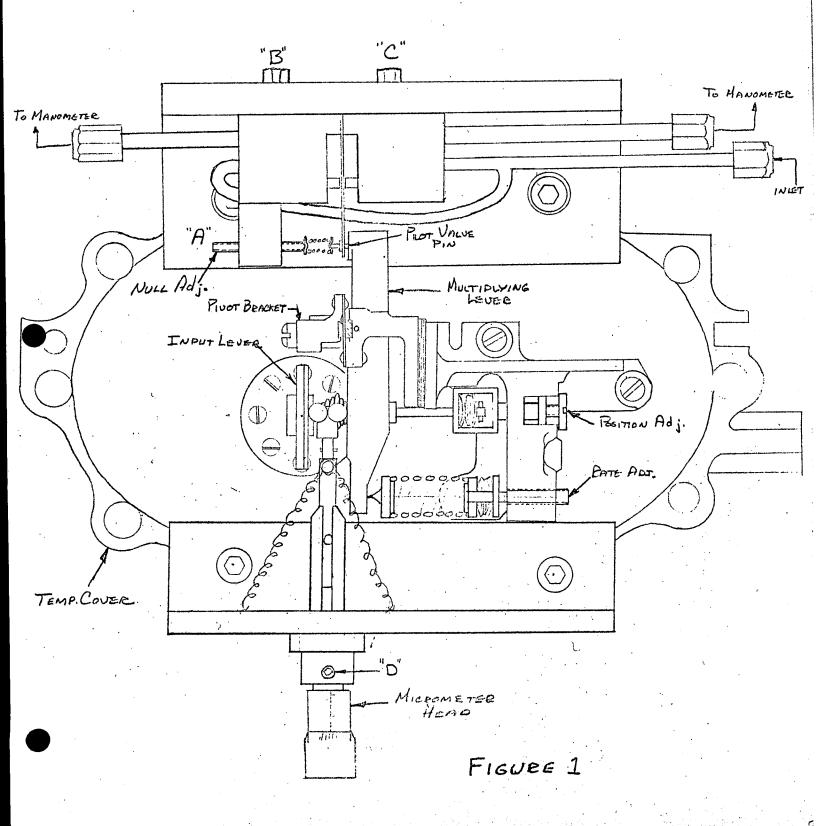
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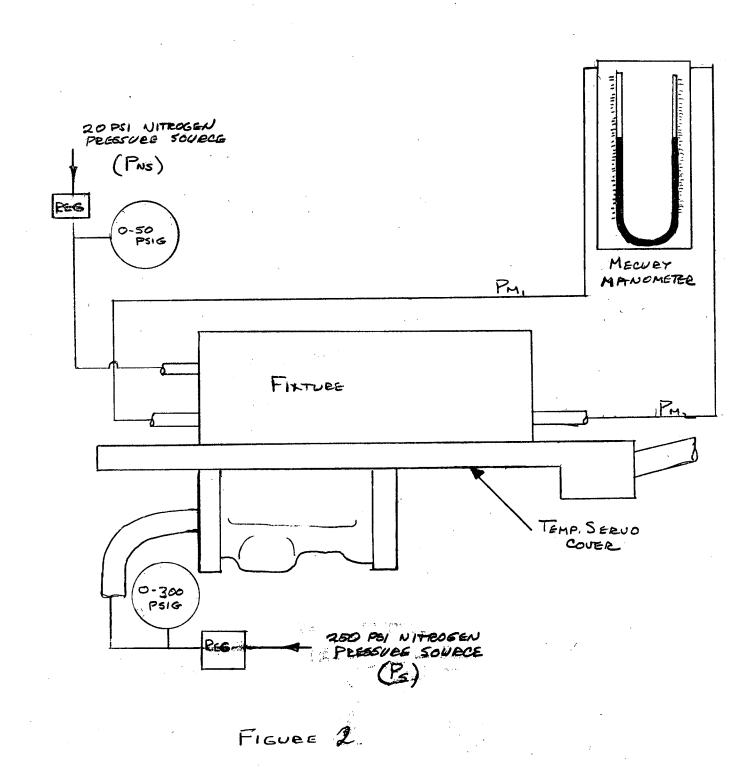
- 2.3.1 Average the hysteresis reading for each roller position for both room temperature data and high temperature data and plot both sets of data on the same sheet per the sample Curve of Appendix B. If the high temperature curve coincides with the room temperature curve, calibration is acceptable and the Tt2 cover assembly may be installed in the control as is.
- 2.3.2 If the high temperature curve falls above the room temperature curve, bimetallic discs must be removed from either the rate adjustment or position adjustment. If the high temperature curve falls below the room temperature curve, bimetallic discs must be added to either the rate adjustment or position adjustment.
- If the plotted data reveals a constant shift in pressure for each roller 2.3.3 position, bimetallic discs could be added to or subtracted from the Position Adjustment. Each disc in the position adjustment has the effect of shifting the curve .65 psi. For Example (Ref. Appendix B) Curve 2 has a shift in pressure of 1.5 psi to the high side. By dividing 1.5 by .65  $(\frac{4}{5})$  = 2.3) we find that it is necessary to remove 2 bimetallic discs in order to lower the curve to coincide with the room temperature curve.
- 2.3.4 If the plotted curve reveals a varying shift in pressure from one end of the curve to the other, bimetallic discs will have to be added or subtracted from the Rate Adjustment. To determine the amount of bimetallic discs to be added or subtracted from the rate adjustment determine the pressure shift in the curve at 73.5 psi. At this point on the curve, one disc has the effect of shifting the curve 1.4 psi (2.2 1.57) we find that it is necessary to add 2 bimetallic discs to the rate adjustment in order to raise the curve to coincide with the room temperature curve.
- .2.3.5 There may be cases where the shift in calibration due to temperature is caused by the incorrect number of bimetallic discs in both the position and rate adjustments. In cases such as this, careful examination of the plotted data should reveal the extent to which each adjustment need be corrected. A trial and error method may have to be employed to correct the above situation.
- 2.4.0 After determining the correct amount of bimetallic discs to be added or removed from the rate and/or position adjustments, recalibrate the Tt2 servo assembly per HS 1503A and return the unit to test.

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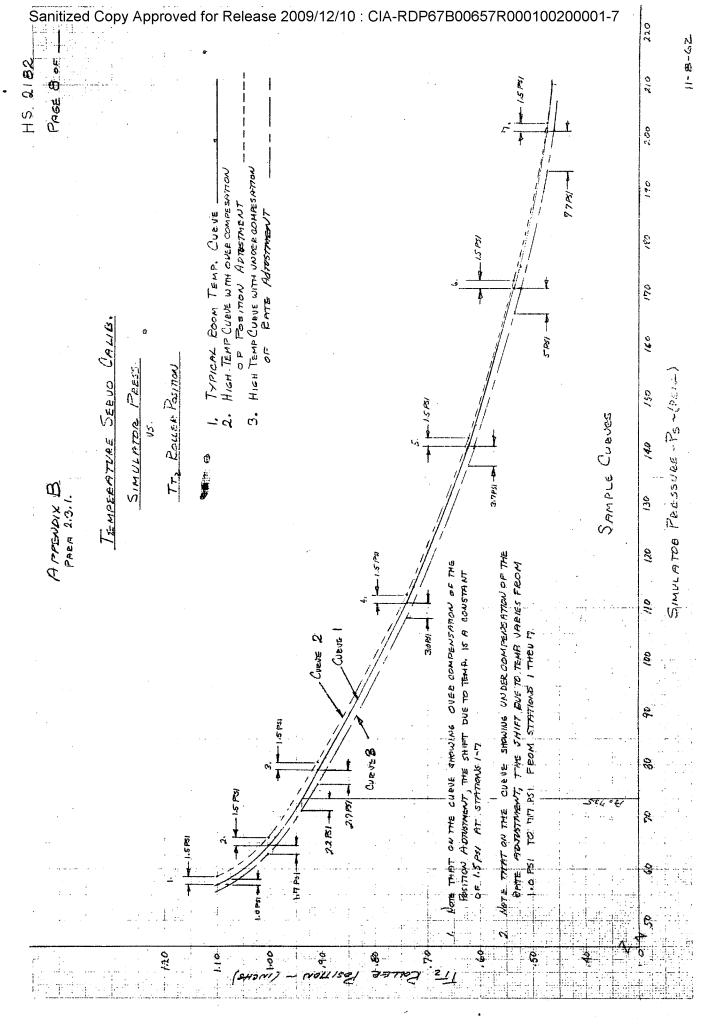
APPENDIX A

Para. 2.2.1

Calibration of Tt2 Sensor

t2 Roller Position (inches)	Simulat	or Pressure Record	(psig)		erature <i>coeo</i>
1.10		Manual 100 % 100			*
1.05					
1.00 .95			*		
.90 .85			4.5		
.85		, suit			
.80 •75			••		
.70	e* ** * * *				*
.65 .60			,		•
•55	•				:
.50 .45					
<b>.</b> 50				,	
•55			•		
.60 .65		,	•		
.70	- # 1 #				
.75 .80			arri S		
<b>.</b> 85					
.90 .95					•
1.00				1	

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1.0 GENERAL INFORMATION

1.1 SCOPE

- 1.1.1 This specification covers the method of calibrating and testing the JFC-47 Exhaust Nozzle Control.
- 1.2 EQUIPMENT REQUIRED
- 1.2.1 A pressure regulating valve, 580888 or equivalent, capable of maintaining regulated pressure at:
  - 1. 1000 ± 70 psi above drain pressure over a flow range of 450-1500 pph.
  - 2. 1000 ± 10 psi above drain pressure while the ENC is operated steady-state at its mid-position.
  - 3. 1000 ± 50 psi above drain pressure while the ENC is being frequency response tested.
- 1.2.2 A 12,000 pph capacity flow bench consisting of a boost pump, an interstage pump and a main pump. The discharge pressure from the boost pump and the interstage pump shall be 40 ± 5 psi and 150 ± 15 psi, respectively. The main pump shall be capable of maintaining:
  - 1. A supply pressure of 2900 ± 100 psi above interstage pressure during steady state ENC operation.
  - 2. A mean supply pressure of 2800 ± 200 psi above interstage pressure during ENC frequency response testing.
  - 3. A maximum peak to peak pressure variation of 1000 psi during ENC frequence response testing.
  - NOTE: Two properly functioning Lucas Rotox 1A389AMSSV5 pumps in parallel with a one quart accumulator charged to 1500 psig will meet this requirement.

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- 1.2.3
- A friction loading device to simulate the force required to move the engine exhaust nozzle. The fixture must meet the requirement of ETG 2798; namely it must have a loading actuator capable of applying a 40-15,000 lb. friction load on a 230 lb. plate which in turn is connected to a 3000 psi hydraulic actuator. The area of the hydraulic actuator is to be approximately 7.44 square inches on the closing side and 6.02 square inches on the opening side, and the stroke is to be 9.0 inches. The feedback arm from the actuator to the ENC is to be 8.32 inches long when the actuator is at mid-position. A 10% deviation in area is permissible provided that a corresponding change is made in the length of the feedback arm and in the total stroke in order to maintain the correct angular feedback change for a given actuator volume change.
- 1.2.4 Two pressure relief valves to limit inlet pressure (PhI) to 3400 psi and body pressure (phc) to 320 psi.
- 1.2.5 Pressure gages with the following ranges and accuracies:
  - 1. Three gages 0-4000 psi with # 1.0% accuracy.
  - 2. Two gages 0-1500 pai with ± 0.25% accuracy.
  - 3. Three gages C-400 psi with # 0.25% accuracy.
  - 4. One gage C-1000 psi with # 0.25% accuracy.
  - 5. One gage 0-100 psi with # 0.5% accuracy.
  - 6. One gage 0-50 psi with # 0.5% accuracy.
- 1.2.6 One flow meter with a 20-500 pph range and an accuracy of 1.0%.
  Two flow meters with a 50-2000 pph range and an accuracy of 1.0%.
- 1.2.7 Orifices with the following flows and accuracies at 500 psi differential pressure or equivalent:
  - 1. Two orifices, O1 and O2, capable of flowing 540 f 15 pph.
  - 2. One orifice, 03, capable of flowing 620 ± 3 pph.
  - 3. One .040 orifice. Og.
- 1.2.8 Two filters, 3000 pai Purolator type 412-5 or equivalent, with 10 micron elements.
- 1.2.9 A protractor fixture, 569455-T-21 to mount on the control feedback shaft, 557111. The protractor must have a ±30 degree range with markings in at least one degree increments with an accuracy of ±0.25 degree. The fixture must be capable of referencing mid-area as determined by the indexing hole in the control shaft cover, 573334.

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1.2.10	A fixture to apply a 11.6 lb.load for calibration of the half-area plunger. Ref. HS 1572 - Sminning Fixture 571575-T-2.			
1.2.11	A fixture, 544900-ET-64 or equivalent, to set the proximity damper adjustment, 576782.			
1.2.12	A 12 ft. stainless steel transmission line with a C.18 inch inside diamet			
1.2.13	Stainless steel lines from the ENC to the two sides of the actuator. The fluid volume must be 33.9 in.3 on the closing side and 29.6 in.3 on the opening side.			
1.2.14	A cycling valve at the end of the transmission line dapable of sinusoids varying its effective area veryons time at a rate of 1-5 cps. The valve be capable of meeting the requirements outlined in Appendix I.			
1.2.15	A four channel Samborn resorder or equivalent position, transducer position, control inlet			
1.2.16	A pressure Drop Controller Arsembly, 580710 o	r equivalent, to maintain		
1.3	Symbols	• .		
1.3.1	The following symbols are used in this specif	ioutions .		
	Phl - Control Inlet Pressure	(psig)		
	Pr - Regulated Pressure	(paig)		
	Phil - Metered Pressure	(paig)		
	Phm2 - Metared Pressure	(paig)		
		(paig)		
	Phs - Servo Pressure			
	Ptx - Transmission Line Pressure	(paig)		
·	Ptx - Transmission Line Pressure Pho - Drain Pressure	(paig)		
	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure	(pais) (pais) (paig)		
,	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure	(Paig) (paig) (paig) (Paig)		
	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure A Ptxo - Differential Pressure (Phx-Pho)	(pais) (pais) (paig)		
	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure A Ptxo - Differential Pressure (Phx-Pho) A Pha - Half area piston differential	(Paig) (Paig) (Paig) (Paig) (Pai)		
	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure A Ptxo - Differential Pressure (Ptx-Pho) A Pha - Half area piston differential Pressure (Pr-Ptx)	(paig) (paig) (paig) (pai)		
	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure A Ptxo - Differential Pressure (Ptx-Pho) A Pha - Half area picton differential Pressure (Pr-Ptx) Wftx - Transmission Line Flow	(Piss) (pois) (pois) (poi) (poi) (poh)		
	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure A Ptxo - Differential Pressure (Pbx-Pho) A Pha - Half area piston differential Pressure (Pr-Pha) Wftx - Transmission Line Flow Wfho - Drain Line Flow	(Piss) (pois) (poi) (poi) (pph) (pph)		
	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure A Ptxo - Differential Pressure (Pbx-Pho) A Pha - Half area piston differential Pressure (Pr-Phz) Wftx - Transmission Line Flow Wfho - Drain Line Flow Wfhn - Interstage Flow	(Pig) (poig) (poig) (poi) (poi) (pph) (pph) (pph)		
•	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure A Ptxo - Differential Pressure (Phn-Pho) A Pha - Half area piston differential Pressure (Pr-Phn) Wftx - Transmission Line Flow Wfho - Drain Line Flow OBD - Overboard Drain Leakage	(paig) (paig) (paig) (pai) (pai) (pph) (pph) (pph) (pph) (drops/min.)		
	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure A Ptxo - Differential Pressure (Ptx-Pho) A Pha - Half area picton differential Pressure (Pr-Pha) Wftx - Transmission Line Flow Wfho - Drain Line Flow Wfho - Interstage Flow OBD - Overboard Drain Leakage FSA - Feedback Shelt Ang.e	(Paig) (paig) (paig) (paig) (pai) (pai) (pph) (pph) (pph) (pph) (degrees)		
	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure A Ptxo - Differential Pressure (Ptx-Pho) A Pha - Half area pieten differential Pressure (Pr-Ptx) Wftx - Transmission Line Flow Wfho - Drain Line Flow Wfho - Drain Line Flow OBD - Overboard Drain Leakage FSA - Feedback Shalt Angle FL - Friction Lead on Astractor	(paig) (paig) (paig) (paig) (pai) (pai) (pph) (pph) (pph) (pph) - (drops/min.)		
	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure A Ptxo - Differential Pressure (Ptx-Pho) A Pha - Half area picton differential Pressure (Pr-Ptx) Wftx - Transmission Line Flow Wfho - Drain Line Flow Wfho - Drain Line Flow OBD - Overboard Drain Leakage FSA - Feedback Shelt Angle FL - Friction Lead on Apthator PDC - Pressure Drop Controller	(prig) (p		
1.41	Ptx - Transmission Line Pressure Pho - Drain Pressure Pho - Cavity Drain Pressure Phn - Interstage Pressure A Ptxo - Differential Pressure (Ptx-Pho) A Pha - Half area pieten differential Pressure (Pr-Ptx) Wftx - Transmission Line Flow Wfho - Drain Line Flow Wfho - Drain Line Flow OBD - Overboard Drain Leakage FSA - Feedback Shalt Angle FL - Friction Lead on Astractor	(paig) (paig) (paig) (paig) (pai) (pai) (pph) (pph) (pph) (degrees)		

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1.4.2 The drain pressure relief valve, RVI, and the inlet pressure relief valve, RV2, shall be set to relieve at 320 psig and 3400 psig, respectively.

1.4.3 The test fluid shall be in accordance with PMD 9073 and maintained at 95 25°F for purposes of this rest.

The control component shall have been shimmed in accordance with HS 1572.

1.5 Inspection Requirements

1.5.1 The items marked with an asterisk (\*) in this specification are RED inspection items and as such must be under inspection surveillance by RED. The steady-state acceptance test and the dynamic response acceptance test, paragraphs 4.0 and 5.0, respectively shall be subject to FEMA cource inspection.

2.0 HAIF-AREA PISTON CALIBRATION

2.1 <u>Installation</u>

2.1.1 Octain a 571576 half-area piston housing that has been assembled per paragraph 4.2 of HS 1572 and plumb per figure 1.

2.2 <u>Calibration Procedure</u>

2.2.1 Supply 1040 psig to inlet of test fixture. Adjust valve V<sub>20</sub> to make Pho equal to 40 psig. Record transmission line pressure (Ptx). If Ptx is not equal to 540 ±3 psig, then enter-figure 2 at recorded Ptx and determine amount of shims that must be added or subtracted. Make the appropriate shimming change as outlined in paragraph 4.2.5 of HS 1572A.

#2.2.2 Repeat step 2.2.1 until the following conditions are met:

Pr = 1040 psig Pho = 40 psig Ptx = 540 ± 3 psig

#2.2.3 The half-area piston stop is shimmed as follows:

1. Set the conditions of paragraph 2.2.2.

2. Slowly turn screw clockwise on cover fixture 571575-T-9 until the fuel flow just begins to change.

3. Remove cover fixture and obtain distance "A" from cover mounting surface to bottom of the adjusting screw.

4. Shim cover 575983 with 571577 shims until distance from the cover mounting surface to the 575982 stop is "A"+ (.028" to .030").

2.2.4 Return the half-area piston housing to the assembly floor for completion of assembly per HS 1572.

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- 3.0 EXHAUST CONTROL CALIBRATION
- 3.1 <u>Installation</u>
- Install the control feedback shaft protractor. Set the pointer on the shaft and rotate until the indexing hole in the pointer is over the indexing hole in the shaft cover. Insert the indexing pin. Adjust the protractor until the pointer is in the line with 0°. Then secure the protractor in place.
- 3.1.2 Mount the control on fixture 571575-T-1 and plumb control as per Figure 3. Remove the indexing pir.
- 3.2 Proof Pressure
- 3.2.1 With the use of an air hose, remove all traces of fluid from the external surface of the control.
- 3.2.2 Close valves V2 and V4 and open valve V5.
- 3.2.3 Adjust VI and maintain the following conditions for a period of five minutes.

Phl = 3050 psig. min. Pr = 3050 psig. min. Phc = 300 ± 10 psig FSA = 0\*

There must be no external leakage and a maximum of 10 drops per minute to overboard drain (Ref. Paragraph 5.4.3). If the control exhibits leakage it is recommended that paragraph 3.3 be completed and that the control be checked for hysteresis prior to disassembly. The hysteresis must not exceed 2.0 degrees, in feedback shaft angle.

- 3.3 <u>Calibration Procedure</u>
- 3.3.1 Open valves V1, V2 and V4 and close valve 5.
- 3.3.2 Set Phl at 3050 psig, Pho at 40 psig, Pr at 1040 psig, and Pho at 90 psig using valve VI. Maintain Wftx at 620 pph while the feedback shaft is adjusted until Phml = Phm2. Ptx must be 540 ± 3 psig. If Ptx is not within the pressure limits, remove cover 571561 and adjust screw 579283-1.

Caution: Locking screw, 579283, must be loose when turning or attempting to turn the adjusting screw 579283-1.

3.3.3 Adjustment:

Increase Ptx: CCW Decrease Ptx: CW

One turn of the adjusting screw will change Ptx approximately 30 psi.

3.3.4 Maintain the committions of paragraph 3.3.2 and adjust locknut 69512-4 until Phml = Phm2 at a feedback shaft angle of 0°.

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### Hamilton Standard ON/BION OF UNITY WINDSOR LOCKS, CONNECTICUT . U.S.A.



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3.3.5 Adjustment:

To change FSA clockwise: CW To change FSA counterclockwise: CCW

One turn of the locknut will change the FSA approximately 6°.

\*3.3.6 Repeat paragraphs 3.3.2 and 3.3.4 until the following conditions are met without readjustment.

Phl = 3050 ±100 psig

Pr = 1040 psig

Pho = 40 psig

Phml - Phm2

FSA - O

Ptx =  $540 \pm 3$  psig

Phc = 90 ±5 psig

Wftx = 620 pph

If the above conditions cannot be met, it will be necessary to recheck the shimming operation as outlined in paragraph 4.5 of HS 1572.

- 3.3.7 The installation torque of the 69512-4 locknut along the threads of 576826 and of the 579283-1 adjusting screw through the helicoil mid-grip in lever 573183 must be 2.0-13.0 in.1bs. when the final adjustments have been completed. Torque lock screw 579283-2 to 8-12 in. lt. greater than the torque recorded at assembly an lockwire with MS20995020.
- 4.0 STEADY-STATE ACCEPTANCE TEST
- 4.1 <u>Installation</u>
- 4.4.1 Remove plug AN814-10CL and install test fitting 571575-T-14. Plumb servo cavity to a 1500 psi gage.
- #4.2 Pilet Valve Saturation Check
- 4.2.1 Set the following conditions:

Phl = 3050 ±100 psig

Phn = 150 ±15 psig

Pho = 40 ±5 psig

Pr = 1040 ±10 psig

Pho = 90 ±5 psig

Wftx = 620 pph

- Vary transmission line flow and feedback shaft angle in the following sequence: max. flow, nominal flow, and minimum flow and -30°, 0° +30° respectively. The limits specified in Appendix B must be met.
- 4.2.3 Remove the test fitting and re-install the ANSI4-100L plug

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\*4.3 Transmission Line Schedule

4.3.1 Open valves V1, V2, and V4 and set the following conditions:

Phl = 3050 ±100 psig

Pho = 40 ±5 psig Pr = 1040 psig

Phc = 90 ±5 psig

4.3.2 Vary transmission line valve, V2, and FSA in accordance with Appendix C to establish null point (Phml = Phm2) at each specified valve configuration. The FSA values must fall within the limits specified in Appendix C.

5.0 DYNAMIC RESPONSE ACCEPTANCE TEST

5:1 Installation

Mount the control on the friction loading fixture, ETG 2798, install regulator, and plumb the control as outlined in Figure 1. Assert, all drains except main pilot valve drain may be routed to atmosphere if desired.

Remove the AN 814-8 CL plug from the damper housing, back off on the 69512-4 locknut, and install the damper adjusting fixture 544900 Et-64. Close valve V7 and open valve V6.

5.2 Damper Setting

5.2.1 Set the following conditions:

Phas = 90 ±5 psig

phl = 3050 ±100 psig

Pho = 40 ±5 psig

Phn = 150 215 psig Pr = 1000 ±10 psig

Ptx = 540 ±10 psig

FL = 0 lbs.

5.2.2 Engage the damper adjusting fixture and slowly turn clockwise until the 230# plate begins to drift towards increase area.

5.2.3 Turn the damper adjustment .0045\* counterclockwise.

5.2.4 Rapidly change Ptx several times from 540 psig to minimum pressure in order to parallel the damper plates.

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5.2.5 Repeat paragraphs 5.2.2, 5.2.3, and 5.2.4.

\*5.2.6 Hold the adjusting screw securely with the adjusting fixture and apply a torque of 30-35 in. lbs. on the 69512-h lockint.

NOTE: Prior to locking the 69512-4 lockmut, the nut and the adjusting screw must have an installation torque (torque required to move the nut along the 576782 screw and also the 576782 screw through the helicoil mid-grip in the 576818 housing) of 2.0-1300 in. lbs.

5.3 Frequency Response Check

5.3.1 Set the conditions of paragraph 5.2.1 and close all pressure gages.

Apply simusoidal metions to the transducer valve at frequencies of 1,2, and 4 cps. The amplitude of the input signal must be adjusted such that the amplitude of the actuator is 1.0 ±0.1 inch peak to peak. Record the following on a four-channel Sanborn:

Frequency CPS	Paper Actuator Speed Amplitud MM/SEC inch		Transdacer Position inch	Ph1 psig	Pr paig
<b>, 1</b>	25	1.0±0.1	Record	Record	Record
2	50	1.0±0.1	Record	Record	Record
L ·	100	1.0±0.1	Record	Record	Record

\*5.3.3 With the frequency response checked in accordance with section 5.3.2, the actuator position must not lag the transducer position by any more than the following values:

Frequency CPS		Max Phase Lag Degrees
1 2 4		40 55 90

#5.3.4 Adjustments

1. Re-adjust the damper .000 COW if the phase lag is greater than the maximum allowable value and repeat paragraphs 5.3.1, 5,3,2, and 5.3.3.

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- 2. Re-adjust the damper .0005 CW if there are any signs of 120 cps instability or 30 cps shutter on the Sanborn traces and repeat paragraphs 5.3.1, 5.3.2, and 5.3.3.
- 5.3.5 Remove the adjusting fixture and install the AN Blu-BCL plug.
- \*5.4. External and Overboard Drain Leakage
- 5.4. I With the use of an air hose, remove all trases of fuel from the external surface of the control.
- 5.4.2 Close valves V2 and Vh and set Valve V1 to obtain the following conditions for a period of five minutes.

Phl 3050 psig min.

10h0 psig min.

= 1000 paig min. Ptx

165 ±10 psig Pho

- There must be no external leakage and a maximum of 10 drops per minute to 5.4.3 overboard drain. The term "no leakage" shall be defined as the permissible visual appearance of fluid on the external surface of the control which does not become progressively greater during the prescribed period of time of this test (5 minutes) to such a degree that fluid runs off the surface of the control or forms droplets.
- 5.4.A With valve V6 in its nermally epsh position, open valve V7 and pressurize the exhaust nessle control for normal operation. Slewly close valve V6 until Phd is 10 psig. Maintain conditions for a period of five minutes. Record any leakage by the feedback shaft.
- PREPARATION FOR STORAGE AND SHIPMENT 6.0
  - Upon completion of test the control shall be lockwired and prepared for storege 6.1 and shipment in accordance with HS1572 paragraphs 4.10.2, 5.0, and 6.0.

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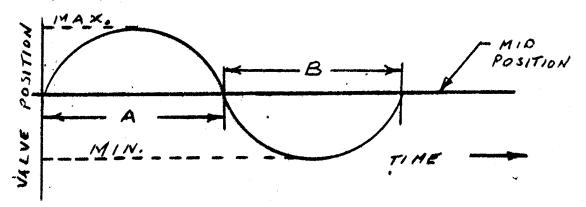
#### APPENDIX A

#### CICLING VALVE REQUIREMENTS

- 1. The valve linearity shall be obtained as follows:
  - a. Maintain a 500 ± 5 psi differential pressure across the cycling valve.
  - b. Displace the valve in 25 pph increments between 525 pph and 725 pph and record valve displacement at each flow setting.

The valve shall be linear within ±3% of the total stroke required to change fuel flow from 525 pph to 725 pph.

- 2. The harmonic content (wave destortion) shall be determined by cycling the valve at 4.0 ± 0.2 cps. The resolved valve position versus time trace must meet the following requirements:
  - a. Symmetry.



a.l Détermine the mid-position from

- a.2 Then determine time "A" and time "B".
- a.3 The factor A/B must be between 0.85 and 1.18.

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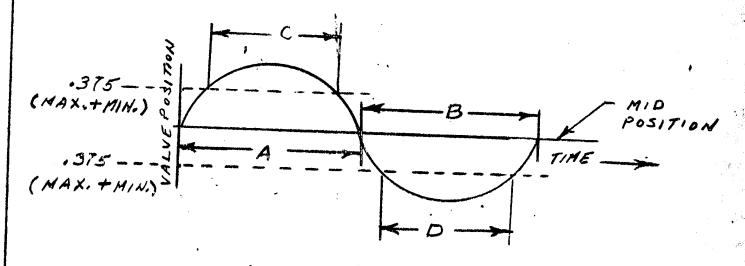
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2. (continued)

b. Wave Shape



- b.1 Draw lines at ± 0.375 (MAX + MIN) from mid-position.
- b.2 Measure the times C and D as shown.
- b.3 The factors C and D must be between 0.19 and 0.27.

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### APPENDIX B

	Wftx pph	Ptx psi	FSA deg.	Phs psi	Wfho pph	Wfhn pph
1.	max flow	200 max Record	<del>-</del> 30	380 max Record	Record	Record
2.	620±3	540±10 Record	0	Record	100-150	800 pph max Record
3.	0	1000 min Record	+30	800 min Record	Record	Record

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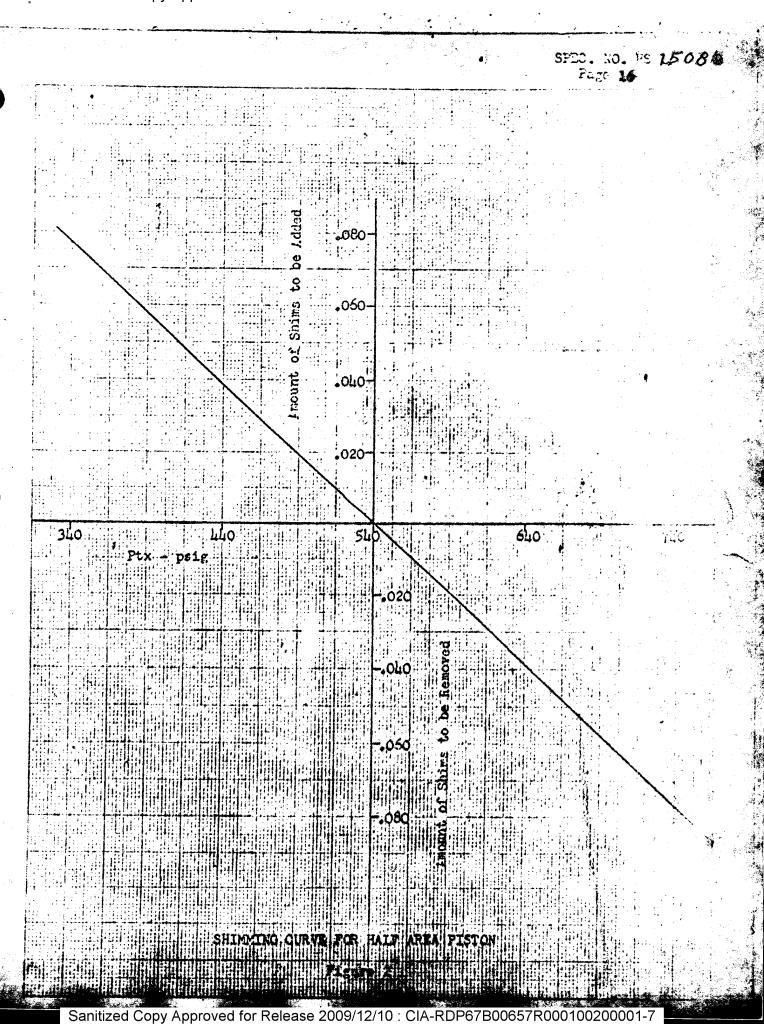


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#### APPENDIX C

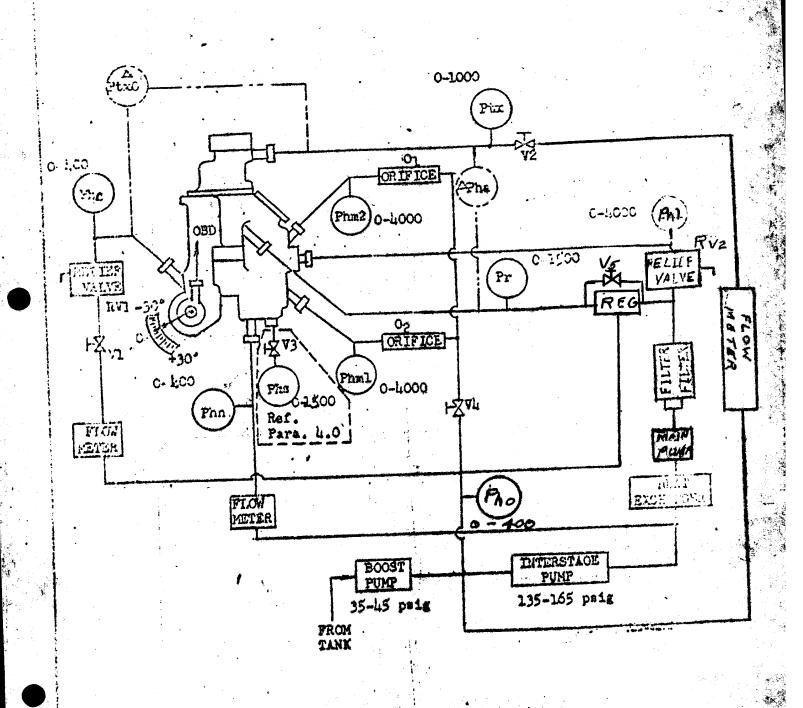
	Wftx pph	Direction of Approaching FSA	FSA Degrees	Ptx -psi
1.	620±3	Inc.	· 0±1	Record
2.	362±2	Inc.	17 to 27 degrees greater than #I	Ħ
3.	620±3	Dec.	O to 2 degrees greater than #I	Ħ
4.	905±5	Dec.	17 to 27 degrees less than #3	*
5.	1120±15	Dec.	-30 to -50 degrees or Phml >Phm2 at min. angle	н
6.	125±5	Inc.	+30 min or Phm2 Phm1 at max angle	*



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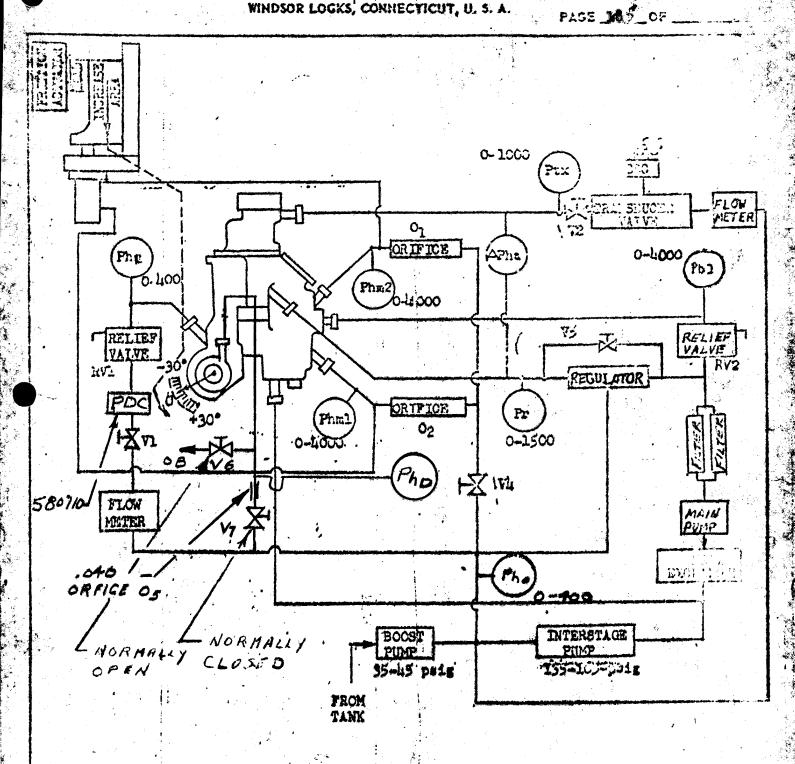
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## HAMILTON SMANDARD DIVISION OF UNITED AURCRAFT CORPORATION WINDSON LOCKS, CONNECTIGUT

H.8. 1508D

Amend. /
Page 1 of 1:
E.C. 72506

Date: /0 3 62

H.S. 1508D, EXHAUST NOZZLE CONTROL - JFC47, CALIBRATION AND ACCEPTANCE OF

	Amendment	! 	1.		:
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- 1. Change paragraph 5.3.2 from:
  - #5.3.2 Apply sinusoidal motions to the transducer valve at frequencies of 1, 2, and 1, cps. The amplitude of the input signal must be adjusted such that the amplitude of the actuator is 1.0 ±0.1 inch pack to peak. Record the following of four-channel Sanborns

Frequency CPS	Paper Speed MM/SEC	Actuator Amplitude inch	Transducer Position inch	Phi psig	Pr psig
1	25	1.0 ± 0.1	Record	Record	Record
2	50	1.0 ± 0.1	Record	Record	Racord
. 4	100	1.0 ± 0.1	Record	Racord	Record

#### to read:

Apply sinuscidal motions to the transducer valve at frequencies of 1, 2, and 4 cps. The amplitude of the input signal must be adjusted such that the amplitude of the actuator is 1.0 ±0.1 inch peak to peak.

Record the following on a four-channel Sanborn:

Frequency CPS	Paper Speed MM/SEC	Actuator Amplitude inch	Transducer *. Position inch	Ph1 * paig	Pra
1	25	1.0 ± 0.0	Record	Record	Becord
2	50	1.0 ± 0.1	Record	Record	Record
4	100	1.0 ± 0.1	Record	Record	Record

\* These items must be recorded on the Sanborn trace. However it is not necessary that they be recorded on the log sheets.

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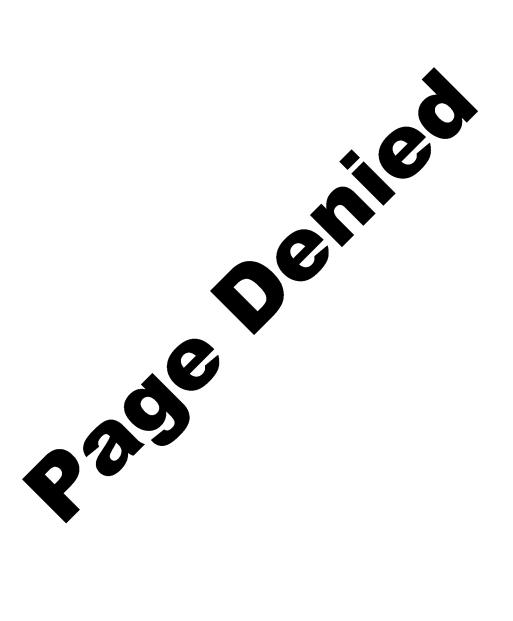
H.S. 1508D "EXHAUST NOZZLE CONT. - JFC47 CALIBRATION ACCEPTANCE OF.

### Amendment 2

- 1. Change paragraph 5.1.1 from:
  - Mount the control on the friction loading fixture, ETG2798, install regulator, and plumb the control as outlined in Figure 4, except, all drains except main pilot valve drain maybe routed to atmosphere if desired.

to read:

Mount the control on the friction loading fixture, ETG2798, install regulator, and plumb the control as outlined in Figure 4 except, all drains except main pilot valve drain must be routed to atmosphere.



### HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT, U. S. A.

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- This specification covers the acceptance and testing of the fuel 1.1 adjustment remote trimmer for the JFC47 fuel control.
- Applicable Drawings 2.0
- The configuration and dimensions of the remote trimmers shall be as 2.1 shown on the applicable Hamilton Standard drawing.
- 3.0 REQUIREMENTS
- Equipment Requirement 3.1
- Test Bench 3.1.1

Acceptance testing of this remote trimmer requires a test bench with the following equipment and/or capabilities.

### 3.1.1.1 Fuel Supply

A fuel source capable of supplying 300 PPH at a pressure of 150-500 psig. The fuel temperature is to be maintained at 85 ± 20°F unless otherwise specified.

### 3.1.1.2 Flow Meter

A flow meter with a 0 - 300 PPH range and an accuracy of 2% of point.

### 3.1.1.3 Gages

- (a) One inlet pressure gage with a range of 0 500 psig, and an accuracy of ±2% full scale.
- (b) One 0 300 psi differential gage with 2% accuracy.

### 3.1.1.4 Pressure Relief Valve

A relief valve capable of limiting pump outlet pressure to 500 psig.

### 3.1.1.5 Power Supply

A power supply of 208  $\pm$  5% VAC, 400  $\pm$  80 CPS, 3 phase shall be available.

#### 3.1.1.6 Test Fixtures

- (a) A remote trimmer mounting block, similar to ETG 2465
- (b) Test fixture metallic seals or equivalent as follows:

One (1) 69400-A21 One (1) 69400-A36

One (1) 69397-A19

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### 3.1.2 High Temperature Test Bench

A test bench similar to that required in Paragraph 3.1.1 but capable of operating at 450°F with PWA523B fuel.

#### 3.2 General Test Requirement

#### 3.2.1 Test Fluid

The test fluid shall be in accordance with FWA523B and maintained at  $85 \pm 20^{\circ}$  unless otherwise specified.

#### 3.2.2. Power Supply

The 208 VAC power supply shall be capable of being directed to either of two pins of the remote trimmer electrical connector by means of a 3 position switch.

### 3.2.3 Abbreviations, Units, and Setting Accuracies

The following is a list of abbreviations (symbols) used in defining remote trimmer performance parameters. All readings, or settings, are to be held to the accuracies listed, unless otherwise specified:

•			a	Full Scale Measurement
Parameter	Symbol	Units	Bet Within	Accuracy
Inlet Pressure	Pin	psig	±5	±2%
Pressure Differential	A P	psi	<b>***</b>	±2%
(Pin-PD) Fuel Flow	Wf	PPH	සා <b>යා</b> දව <del>-</del>	±2%
Drain Pressure	PD	psig -	±2	±2%

### 3.2.4 Plumbing

The test plumbing requirements are defined on Figure 1, Appendix A.

### 4.0 High Temperature Acceptance Test

### 4.1 Installation

4.1.1 Mount the remote trimmer on test fixture and plumb in accordance with Figure 1, Appendix A.

### 4.2 Torque

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4.2.1 Set Pin = 200 psig, PD = 50 psig, and fuel temperature at 440 ± 10°F. With 208 VAC 400CPS power supplied to the remote trimmer, apply restraining torque to trimmer output shaft until shaft ceases to turn. Check the stall torque in each direction of rotation and record.

NOTE: Duty cycle of the unit at elevated temperature is 5 minutes on, 5 minutes off. During any phase of the High Temperature Acceptance Test, the power shall never be applied for periods longer than 5 minutes. After any 5 minute period of applied power the unit shall be allowed to cool for no less than 5 minutes.

- 4.3 Range and Rate of Adjustment
- 4.3.1 Apply power to the trimmer and determine the number of revolutions for full range of the trimmer and the rate of operation.
- 4.3.2 The full range of trimmer operation shall be  $5 \pm \frac{1}{4}$  turns. Record range.
- 4.3.3 The rate of operation of the trimmer, shall be  $1 \pm \frac{1}{4}$  RPM with 400 CPS power supplied. Record rate.
- 4.3.4 When the range and rate of adjustment have been determined, position the output shaft in the full CCW position when viewed in direction "E" as shown on applicable drawings. Run unit against the full CCW position stop for 10 seconds, set 3 position power switch to DFF, and return unit to room temperature conditions.
- 5.0 ROOM TEMPERATURE ACCEPTANCE TEST
- 5.1 INSTALLATION

Mount the remote trimmer on test fixture ETG 2465 or equivalent, and plumb in accordance with Figure 1, Appendix A.

- 5.2 Leakage Test
- 5.2.1 Set and maintain the following conditions for five (5) minutes:

$$Pin = PD = 385 \pm 15 psig$$

- 5.2.1.1 There shall be no visible external leakage or weepage, except through the overboard drain fitting. Note location if leakage or weepage occurs.
- 5.2.1.2 Overboard drain leakage shall not exceed 1 cc/min. Record actual leakage.
- 5.3 Gooling Flow
- 5.3.1 Set Pin = 200 psig, PD = 50 psig (ref,  $\Delta$  P = 150 psi) and measure flow. Cooling flow shall not exceed 100 PPH. Record actual flow.
- 5.4 Torque

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- 5.4.1 Remove remote trimmer from fixture ETG 2465.
- 5.4.2 Install fixture 20 X 18001 and supply boost pressure to trimmer.
- 5.4.3 With 208 VAC 400 CPS power applied, apply restraining torque to trimmer output shaft until output shaft ceases to turn. Check each direction of rotation.

Note: Duty cycle of the unit is 10 minutes on, 10 minutes off.

During any phase of this acceptance test, the power shall never be applied for periods longer than 10 minutes. After any 10 minute period of applied power the unit shall be allowed to cool for no less than 10 minutes.

- 5.4.3.1 The restraining torque (stall torque) shall be 15-23 inch-pounds. Record stall torque in each direction.
- 5.4.4 If external adjustments are provided, they must be capable of adjustment with 5-45 in# of torque. Record torque required to make external adjustment.
- 5.5 Range and Rate of Adjustment
- 5.5.1 Apply power to trimmer and determine the number of revolutions for full range of trimmer, and the rate of operation.
- 5.5.1.1 The full range of trimmer operation shall be  $5 \pm 1/4$  turns. Record range.
- 5.5.1.2 The rate of operation of the trimmer shall be 1  $\pm \frac{1}{4}$  RPM at 400 CPS power supply. Record rate.
- 5.5.2 In preparation for shipment, position the output shaft in the full CCW position when viewed in direction "E" as shown on applicable drawings.
- 6.0 QUALITY ASSURANCE PROVISIONS
- 6.1 It shall be the responsibility of the remote trimmer manufacturer to conduct an acceptance test of each remote trimmer prior to shipment. As a minimum, this acceptance test must demonstrate conformance with the functional requirements defined in paragraphs 4.0 and 5.0 of this specification.
- 6.2 It shall be the responsibility of the Hamilton Standard Quality Control Department to insure functional compliance of the unit to the requirements specified in paragraphs 4.0 and 5.0 of this specification, and to insure compliance with (MIL-Q-9858).
- 7.0 PREPARATION FOR DELIVERY OR STORAGE
- 7.1 Upon completion of the acceptance test procedure, the remote trimmer shall be drained of all residual fuel and flushed with MIL-E-6081, Grade 1010 oil and equivalent. All openings shall be capped to exclude dirt and other foreign matter, and to protect threaded fittings.

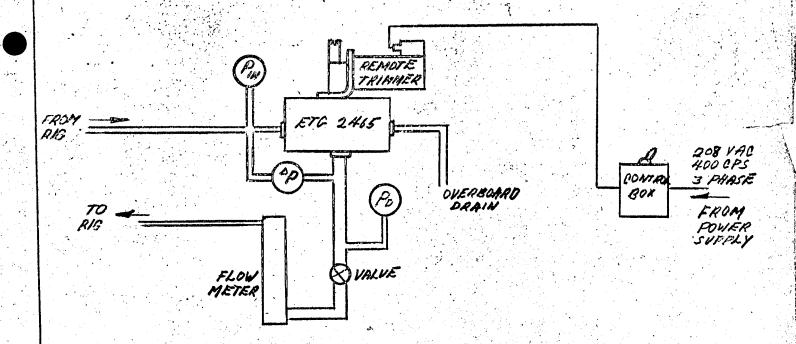
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HS SPEC NO 1350 P

APPENDIX A JFC-47 REMOTE TRIMMER PLUMBING SCHEMATIC





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1.	General Requirements
<b>1.1</b>	Equipment Requirements
1.1.1	Flowbench capable of handling at least 0-4000 PPH flow of PWA 523B at 3000 psig pressure and 90 ± 10°F.
1.1.2	Flow Meter - Range of 300 to 1400 PPH and capable of 200 psi working pressure.
1.1.3	Flow Meter - Range of 0 to 50 PPH and capable of 200 psi working pressure.
1.1.4	One hand valve to set pressure in the regulator discharge line upstream of the Flow meter (transmission pressure) as shown on figure 1.
1.1.5	Pressure Regulator for maintaining drain pressure at 30-155 psi.
1.1.6	Instrumentation for taking the measurements listed below with the accuracy specified:
	Pl Regulator inlet pressure, at least 2000 to 4000 psig pressure range with an accuracy of ±25 psig within this range.
	PR Regulated pressure, at least 500 to 1500 psig pressure range with an accuracy of ±10 psig within this range.
	Wf Fuel flow out of regulator 300 to 1400 pph range with an accuracy of 2% within the range.
	Wif Leakage flow out of drain 0 to 50 pph range with an accuracy of 2% within this range.
	PB Drain pressure, at least 30 to 350 psig pressure range with an accuracy of the psig within this range.
	T Regulator inlet fuel temperature, at least 70° to 110°F temperature range with an accuracy of ±5°F within this range.
1.2	Test Fluid
1.3	The calibration test fluid shall be PMC 9073 for static and dynamic tests and P & WA 523B for hot tests.  Installation
	The regulator shall be mounted on the flow bench in a position similar to its mounting on the engine as shown on figure 1.

The following data shall be recorded on each data sheet.

Data Required

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1.4.1 (continued)

> **A** Regulator Serial No. CC. Test Fluid Type and Specific Gravity BB HSD Parts List and Revision No. D. Test Fluid Temperature

1.4.2 The following data shall be recorded when specified:

Pl Regulator Inlet Pressure

PR Regulated Pressure

Wf Regulated Fuel Flow

Wlf Drain Leakage Flow

PD Drain Pressure

#### 2. Shimming:

- 2.1 Assemble the regulator per applicable blueprint with / 080 shims and plumb on the Rig according to figure 1. With Pl at  $\beta$ 050 psi set Wf by hand valve to read 800 ± 10 pph with PD at 30 psi, NOTE: PR. Determine the thickness of shims necessary to obtain PR = 1070 psi at Pl = 3050 psi, PD = 30 psi and Wf = 800 ± 10pph 43.5 psi/.QOl shim)
- After adding or subtracting the calculated amount of shims, run the 2.2 control again and record regulated pressure. If Pr is not 1079 ± 20 psigreshim per paragraph 2.1.
- 3. Test Procedure
- 3.1 Calibration - Inspection Required

Under flow conditions and with Pl at 3050 ± 10 psi, PD at 30 ± 5 psi, T at 95° to 25°F, set hand valve to obtain the Wf as tabulated by test points in the order listed. Record Pl, PD, Wf and PR for each test point.

est Poi	Int Fl PSIO	Wf PPH	PD PSIG	Limita RR-PSIG
1.	3050:20	400±10	30±5	
2.	3050±20	500±10		550 <b>- 12</b> 0
3.	3050±20	600±10	30±5	950 - 1210
Į.	3050±25	700±10	30±5	950 - 12Jo
4. 5.	3050120		30 <b>±</b> 5	950 <b>- 12</b> 00\\\\\
6.	3050±2)	800±10	30±5	1650 - 1090 1
7.		900±10	30 <b>±</b> 5	950 - 1200
8.	3050+20	1000±10	30±5	950 - 1200
	3050:20	1100±10	30\$5	\$50 <b>- 12</b> 00 \
9.	3050: 20	1200±10	30±5	950 <b>- 12</b> 00
10.	3050± <b>2</b> 0	1000±10	30±5	Middle of and and an
V	Within 20 psig of	f	,02,	Within 25 psig of PR
11.	Pl recorded at	800±10	30±5	recorded at test point 7.
	test point 5	000-200	7027	Within 25 psig of PR
12.	3050±20	600±10	20+4	recorded at test point 5.
	90 <b>9</b> 0.20	AAA=#A	30±5	Within 25 psig of PR
13.	3050:20	LODATO		recorded at test point 3.
-,•	2020.20	400±10	30±5	Within 25 psig of PR

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#### RAMILTON STANDARD

SPEC. NO. HS 14940

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WINDSOR LOCKS, CONNECTICUT, U. S. A.

PAGE 4 OF

(continued) 3.2

> Limits: Regulated pressure must be within the specified limits at each test point.

DRAIN LEAKAGE 3.2

> At the conditions specified in test point 9 of paragraph 3.1, record the drain leakage flow. Leakage flow shall not exceed 20 pph. 20 PFH = 188.5 cc/min or 6.37 oz/min.

EXTERNAL LEAKAGE 3.3

> Completely close the regulated pressure hand valve. Adjust regulator inlet pressure (P1) to 3400 to 3500 psig and drain pressure (PD) to 300 ± 10 psig for a period of at least three (3) minutes. Record Pl, PD, PR, and any external leakage.

Limits: There shall be no external leakage from any portion of the regulator assembly.

Frequency Response Test 3.4

Install the PRV into the test set-up as shown in Figure 2 Page 2.

The pressure transducer should be as close to the PRV as possible.

Adjust valve "C" to obtain 400 ± 25 pph fuel flow with P1 at 3000 ± 20 psig and cycle the cycling valve at 5 cps and at an amplitude such that PI cacillates at an amplitude of 400 t 20 psi peak to peak. Cycling range shall fall within the limits of 2580 - 3020 psig.

Record Wf pph and PR amplitude psi PR limit 20 psi peak to peak max.

Adjust Valve "C" to obtain 1200 ± 25 pph fuel flow with PI at 3000 ± 20 psig and repeat the frequency response at 5 cps, Pl = 400 ± 20 psi peak to peak. The PRV amplitude limit is 20 psi peak to peak max.

HOT FUEL TEST . 3.5

Install the PRV in accordance with Figure 1 on the hot test rig and repeat 3.50% test points 1, 3, 5, 7, 9, 10, 11, 12 & 13 of Para. 3.1.

Carry out the following test at elevated temperatures: 3.5.2

Test Point	P1 (PSIG)	Wf (PM)	Fuel Temp.
1 2 1 1 5	3050 ± 20 3050 ± 20 3050 ± 20 3050 ± 20 3050 ± 20	400 ± 10 600 ± 10 800 ± 10 1000 ± 10 1200 ± 10	450° ± 10° 450° ± 10° 450° ± 10° 450° ± 10°

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### HAMILTON STANDARD

### DIVISION OF UNITED AIRCRAFT CORPORATION

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WINDSOR LOCKS, CONNECTICUT, U. S. A.

3.5.2 .continued)

Limits: There shall be no instability when changing the Wf from the established test point value to the most extreme test point Wf and back to the established test point Wf in an elapsed time of 2 sec. or less (example: 400 pph to 1200 pph to 400 pph; 800 pph to 1200 pph to 800 pph; 1000 pph to 400 pph to 1000 pph; etc.)

3.5.3 After completing the hot test repeat para. 3.5.1.

3.6 Damping Land Leakage Test

Remove the ANSI4 -2SL plug from the base of the PRV and replace with a standard -2 union and set up as shown in Figure 3 Page 3

Carry out the following test:

P\_ psig PD psig Leakage cc/min

3000 Record 2000 (Adjusted by needle Valve D)

Record

h.t) Preservation and Storage

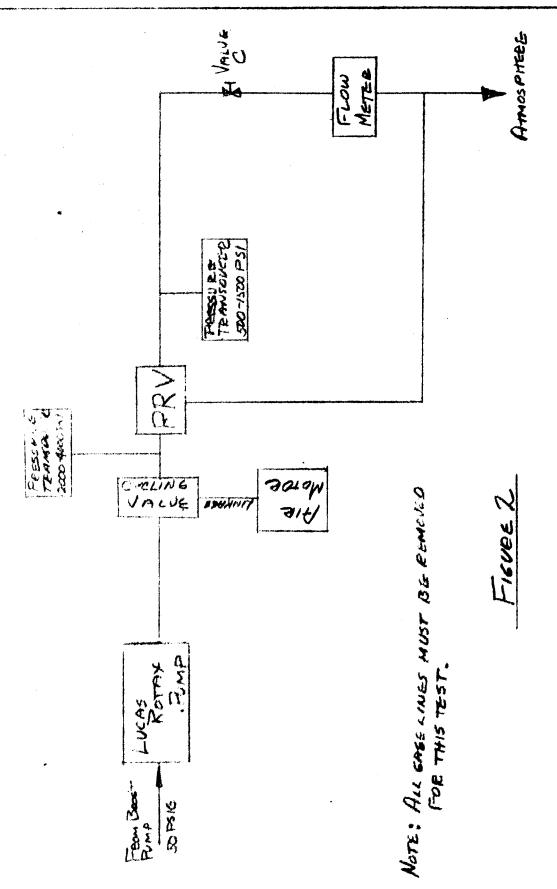
After completion of testing, the regulator assembly shall be drained of fuel and prepared for storage in accordance with HS Spec. No. 380. Protective covers and containers shall be used to prevent damage or contamination of the regulator assembly.

Sau Applicable Figures

Figure I Test Position and Schematic Diagram 4/18/61.

# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT, U. S. A.

SPEC. NO. HS \_\_14940 CODE IDENT NO. 73030 PAGE \_\_7\_\_\_OP \_\_\_\_\_\_\_



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4. Change paragraph 3.6 from:

3.6 "Damping Land Leakage Test

Remove the ANSIA -2SL plug from the base of the PRV and replace with a standard -2 union and set up as shown in Figure 3 Page 3

Carry out the following tests

Pl psig PR . PD psig Leakage cc/min

1 3000 Record 2000 (Adjusted by needle Valve D)

to reads

3.6 "Post Hot Test Calibration Check

Repeat paragraph 3.1.

- 5. Add the following as para. 3.7.
  - 3.7 Remove the ANSIL -2SL plug from the base of the PRV and replace with a standard -2 union and set up as shown in Figure 3 Page\_\_\_\_\_.

Carry out the following tests

Pi psig PR PD psig Leakage cc/min T S000 Resord P000 (Adjusted by needle Valve D)

6. And the attached sheet as Figure ?.

### HAMIETON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT

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# 11940. "PRESSURE REBULATOR - END. JF JLT, CALIBRATION OF"

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- Change the first sentence of paragraph (.) from:
  - 7.4 "Install the PRV into the test second as shown in Figure 2 Page 2.
  - 1.4 "Install the PRT into the test set-up as shown in figure 2 page ?.
- 2. Change paragraph 3.5.1 iron:

to reads

- 3.5.1 "Instail the PRV in accordance with Figure 1 on the hot test rig and repeat test points of Sp Sp Sp 10, 11, 12 & 13 of Para. 3.1.
- 3.5.2. \*Install the PRV in appordance with Figure I on the hot test rig and carry out the following test at elevated temperatures:

fest Point	Pi (PSIG)	Wf (PPH)	Fuel Temperature		
	3050 ± 21 3050 ± 35 3030 ± 35 3030 ± 20 3030 ± 20	400 ± 50 600 ± 50 800 ± 50 1000 ± 50 1200 ± 50	450° ± 25 450° ± 25 450° ± 25 450° ± 25		

- Limitat There shall be no instability when changing the Wf from the established test point value to the most extreme test point Wf and back to the equablished Wf in an elepsed time of 2 sec. or less (example: 400 PPH to 12000 PPH to 4000 PPH; 1000 PPH to 4000 PPH to 4000 PPH; 1000 PPH to 4000 PPH; 1000 PPH; 1000 PPH; 1000 PPH to 4000 PPH; 1000 PPH; 1000 PPH; 1000 PPH; 1000 PPH to 4000 PPH; 1000 PPH; 100
- 3. Detate paragraph 3.5.2 and 3.5.2.

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## HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTIGUT

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H. S. 14940 "PRESSURE REGULATOR - ENC. JFC47, CALIBRATION OF"

Amendment /	
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- 1. Thange the first sentence of paragraph 3.4 from:
  - 1.4 "Install the PRV into the test set-up as shown in Figure 2 Page 2.

    to read:
  - 3.4 "Install the PRV into the test severap as shown in figure 2 page ?.
- 2. Change paragraph 3.5.1 from:
  - 3.5.1 "Install the PRV in accordance with Figure 1 on the hot test rig and repeat test points 1, 3, 5, 7,9, 10, 11, 12 & 13 of Para. 3.1. to read:
  - 3.5.1 "Install the PRV in arrowdance with Figure I on the hot test rig and carry out the following test at elevated temperatures:

Test Point	PI (PBIG)	Wf (PPH)	Fuel Temperature
2. 2. 3.4 5	9050 ± 20 3050 ± 20 3050 ± 20 3050 ± 20 3050 ± 50	400 ± 50 600 ± 50 800 ± 50 1000 ± 50 1200 ± 50	450° ± 25 450° ± 25 450° ± 25 450° ± 25

Limits: There shall be no instability when changing the Wf from the established test point value to the most extreme test point Wf and back to the established Wf in an elapsed time of 2 sec. or less (example: 400 PPH to 12000 PPH to 1200 PPH to 1200 PPH to 1200 PPH; but a local PPH; but a local PPH; but a local PPH; etc.)

3. Deliene paragraph 3.5.2 and 3.5.1.

### HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT

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- 4. Charge paragraph 3.6 from:
  - 3.6 "Damping Land Leakage Test

Remove the ANSIL -2SL plug from the base of the PRV and replace with a standard -2 union and set up as shown in Figure 3 Page 3

Carry out the following test:

Pl psig PR PD psig Leakage cc/min

Record 2000 (Adjusted by needle Valve D)

Record

to reads

3.6 "Post Hot Test Calibration Check

Repeat paragraph j.l

- 5. Add the following as para. 3.7.
  - 3.7 \*Remove the ANSIA -2SL plug from the base of the PRV and replace with a standard -2 union and set up as shown in Figure 3 Page\_\_\_\_\_.

Carry cut the following test:

Pr psig PR PD psig Leakage cc/min
Record 2000 (Adjusted by Record

3000 Record 2000 (Adjusted by needle Valve D)

6. And the attached sheet as Figure ?.

### DIVISION OF UNITED AIRCRAFT CORPORATION

WINDSOR LOCKS, CONNECTICUT, U. S. A.

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BRADUATE M FIGURE OPEN TO ATMOSPHERE HYDRAULIG PUMP

H.S. 14940 Amend. 1 Page 3 of 3 E.C. 73708 Date: 11-16-62

## HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTIGUT

Amend. 2 Page 1 of 1 E.C.A. 74591 Date 1/-24-62

H. S. 1494C - "PRESSURE REGULATOR - ENC, JFC47, CALIBRATION OF"

Amendment 2

Change paragraph 1.2 from:

". . . . shall be P&WA 523B."

To reads

". . . . shall be P&WA 523B containing .ll pounds of P&WA FS67 additive per 50 gallons of fluid."

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3.1.1 With the valve, gages, etc. connected per Figure 4, set the following two conditions separately:

 WFD
 PDS
 PD
 WFS.
 PBS
 PI
 P2

 975-1025
 25-35
 50-55
 80-200
 185 REF
 140 REF
 40-50

 Record Pl
 Pl shall equal 107-113 psi.

Slowly decrease the fuel flow to zero by closing the inlet regulating valve. Observe the valve assembly for evidence of fuel shut off valve chatter. Chatter is defined as opening and closing at the fuel shut off which causes fluctuations in the fuel flow. Audibly snapping of the valve and rapid fuel flow fluctuations shall be considered evidence of chatter and the valve shall be rejected for repair and/or rework.

3.1.2 In order to bring the differential pressure, Pl, within the limits of 107-113 psi, add or subtract shims, P/N 520128, as found necessary on the shutoff valve. (The addition of shims will increase Pl).

#3.1.3 Test Point I:

Upon completion of the shimming of this valve, set and record the following conditions:

				LIMIT	LIMIT	
WFD	PDS	PD	<u>P2</u>	WES	P1.	
975-1025	25-35	50-55	10-50			
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Record the leakage from the bypass standpipe, leakage from the overboard drain, and external leakage over a five (5) minute period.

#3.1.4 Test Point II

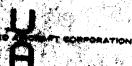
Increase the discharge fl ow to 1675-1725 pph and then to 34,500-35,500 pph set and record the following conditions:

					LIMIT	LIMIT	LIMIT
spec	WFD	PDS	PO	<u>P2</u>	VES	<u>Pl</u>	12
1	1675-1725	170-180	160-170	40-50	80-200	107-113	
2	34,550-35,450	160-170	480-520	40-50		3 19 <b>年</b> 11 - 1	LO MAT

Record the leakage from the bypass standpipe, leakage from the overboard drain, and external leakage over a five (5) minute period. Leakage from the bypass standpipe shall not exceed 5 co per minute at test points I & II. Leakage from overboard drain shall not exceed 50 cc/min for 1000 pph and 50-55 PD test point I and loc/min at test point II. There shall be no external leakage at each test point.

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### Hamilton Standard BY SIGHT OF UNITS WINDSOR LOCKS, CONNECTICUT . U.S.A.



PAGE 2 OF

1.0 SCOPE

- 1.1 This specification covers the method of calibrating and acceptance testing the JFC-47 Windmill Bypass, Check and Dump Valve Assembly.
- 2.0 GENERAL REQUIREMENTS
- 2.1 Equipment Requirements
- 2.1.1 Flow bench capable of supplying at least 1000 to 40,000 pph fuel flow at 900 psig pressure and 2000 pph fuel flow at 1500 psig pressure.
- 2.1.2 Boost Pump, capable of maintaining the stand fuel pump inlet pressure at 25-30 psig over a fuel flow range of 1000 to 40,000 pph.
- 2.1.3 Heat Exchanger to maintain the fuel temperature at the valve assembly inlet within the range of 95 ± 5°F.
- 2.1.h Filter containing 25 to 40 micron element installed in the stand pump discharge line.
- 2.1.5 Test Fittings to adapt to the windmill bypass, check, and dump valve assembly standpipes.
- 2.2 Installation The valve shall be mounted on the flowbench in either test position A or B as specified in Figures 1, 2, 3, or 4.
- 2.3 Instrumentation for taking the measurements listed below with the accuracy specified.
- 2.3.1 Pressure Gages
  - PI Inlet pressure, at least 100-1500 psig pressure range with an accuracy of 1% of full scale.
  - PB Bypass pressure, at least 20-200 paig pressure range with an accuracy of 1% of full scale, and a 50 to 1200 paig gage with accuracy of 15 paige.
  - FD Discharge pressure, at least 50-1200 psig pressure range with an accuracy of 15 psig. When lines are connected per Figure 4 use a 0-200 psig gage 11% full scale accuracy.
  - PDS- Discharge signal pressure, at least 20-200 psig pressure range with an accuracy of the of full scale and at least 100-1000 psig pressure range with an accuracy of the of full scale, depending upon the test set-up.
  - Pi -Differential pressure (PI-PDS) at least 0-150 psi pressure range with an accuracy of 1.5 psi in the range of 107-113 psi.
  - PE Differential pressure (PBS-PI) at least 0-100 psi pressure range with an accuracy of ±.5 psi in the range of 40-50 psi.
  - P3 Differential pressure (PI-PD) at least 0-100 psi pressure range with an accuracy of ±1% of full scale.

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HAMILTON STANDARD

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WINDSOR LOCKS, CONNECTICUT, U. S. A.

PAGE 3 OF

----WFS Signal Fuel Flow (PPH)

2.3.1 Pressure Gages (Continued):

Ph - Differential pressure (PDS-PT) at least 0-100 psi pressure range with an accuracy of ±.5 psi in the range of 40-50 psi.

P5 - Differential pressure (PI-PBS) at least 0-150 psi pressure range with an accuracy of 1.5 psi in the range of 40-50 psi.

PBS-Bypass signal pressure, at least 20-200 psig pressure range with an accuracy of £1% of full scale and at least 100-1000 psig pressure range with an accuracy of £1% of full scale, depending upon the test set-up.

#### 2.3.2 Fuel Flow Meters

Outlet fuel flow, at least 900-40,000 pph fuel flow range with an accuracy of ±1% within this range.

WFS - Signal fuel flow, at least 50-400 pph fuel flow range with an accuracy of ±1% within this range.

- 2.3.3 Fuel Temperature, measure at valve assembly inlet with at least a 80 to 100°F temperature range, with an accuracy of ±2°F. within this range.
- 2.4 Test Fluid shall be PMC9073 at 95 ± 5°F.
- 2.5 Data to be recorded
- 2.5.1 The following data should be recorded on each data sheet:

Valve Assembly Serial Number Valve Assembly Part Number Fuel Type and Specific Gravity Fuel Inlet Temperature

2.5.2 The following data shall be recorded when specified:

PI - Inlet Pressure (psig)

PD - Discharge Pressure (psig)

PB - Bypass Pressure (psig)
PDS - Discharge Signal Pressure (psig)

PBS - Bypass Signal Pressure (psig)

WFD - Discharge Fuel Flow (pph)

WFB - Bypass Fue; First (pph)
Pl - Differential Pressure (psig)

P2 - Differential Pressure (psig)

P3 - Differential Pressure (psig)

Ph - Differential Pressure (psig)

P5 - Differential Pressure (psig)

### 2.6 Inspection Requirement

The items marked with an asterisk (\*) in this specification are HSD inspection items and as such must be under inspection surveillance by HSD.

3.0 TEST REQUIREMENTS

3.1 Sanitized Copy Approved for Release 2009/12/10 : CIA-RDP67B00657R000100200001-

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3.1.5 With the installed per Figure 4 set Pds = 30 ± 5 psig, Pbs = 200 ± 10 psig, Pl 80 ± 10 psig, and Pd 55 ± 5 psig. From this condition set up the following test points in the order shown using test stand inlet control valve and the discharge control valve.

Note: Care should be taken not to overshoot the test points (it may take two or three practice runs before taking final test data).

Record: Inlet press. Pl, discharge press. Pd., fuel flow Wf, and dump overboard valve leakage.

Test Point	Wf pph	Pd psig	Leakage Limit co/min.	
<b>1</b>	1000 ± 25	50 <b>-55</b>	50 Max.	
2	1700 ± 25	160-170	1 Mex.	

3 With the discharge valve closed and the bleed valve open regulate the discharge pressure at 120 ± 10 psig with the inlet by-pass valve.

Now reduce the inlet flow slowly by opening the inlet by-pass valve and observing the discharge pressure (Pd) at which the dump valve opens. For a more accurate reading hesitate at 20 psig Pd to determine if the pressure will bleed down through the bleed valve; if the pressure will not bleed down carefully open by-pass until dump valve opens.

### Limit is 12 paig minimum.

Dump valve opening pressure is defined as the pressure at which the flow suddenly increases from the overboard drain and Pd suddenly decreases. If the discharge pressure will not drop below 12 peig due to test stand boost pressure or pressurised tank then the bleed in the discharge line will have to be opened to apop the pressure until the dump valve opens.

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#### HAMILTON STANDARD

### DIVISION OF UNITED AIRCRAFT CORPORATION

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WINDSOR LOCKS, CONNECTICUT, U. S. A.

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3.2 Windmill Bypass Operation

3.2.1 With the valve, gages, etc connected as in fig. 3, set the following conditions

Wf In	<b>PB</b>	PBS	Pi
1675-1725	107-113	25-35	40-50
Record P5.	P5 shall equal 107-113 psi.		

3.2.2 In order to bring the differential pressure, P5, within the limits of 107-113 psi, add or subtract shims, P/N520128, as found necessary on the bypass valve.

#### 3.2.3 Test Points:

Upon completion of the shimming of this valve set and record the following condition:

•			•	Li	dts
WfB ·	PB	PBS	PL	P5	Wrs
975 <b>-</b> 1025 16 <b>7</b> 5-1725	107 <b>-113</b> 107 <b>-113</b>	25 <b>-</b> 35	40-50	107-113	80-200
spec. 4975-5025	107-113	25-35 135 <b>-1</b> 50	40-50 40 <b>-50</b>	107 <b>-113</b> 107 <b>-113</b>	80-200

Record the leakage from the discharge standpipes, leakage from the overboard drain, and external leakage over a (5) minute period. Leakage from the discharge standpipe shall not exceed 2 cc per minute at each test point. There shall be no external leakage at each test point.

### 3.3 <u>Internal Leakage</u>

With the valve mounted in the test position Figure 2 set the following points: Record inlet pressure PI.

Set	PI	Limits		
#1 #2,/	130-140 520-560	FBS 5 cc/min 5 cc/min	PDS 2 cc/min 2 cc/min	

Record leakage from the discharge signal standpipes and bypass signal standpipe at each point over a 5 minute period, starting at least 1 minute after setting the test point.

### 3.4 External Leakage

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HAMILTON STANDARD

DIVISION OF UNITED AIRCRAFT CORPORATION

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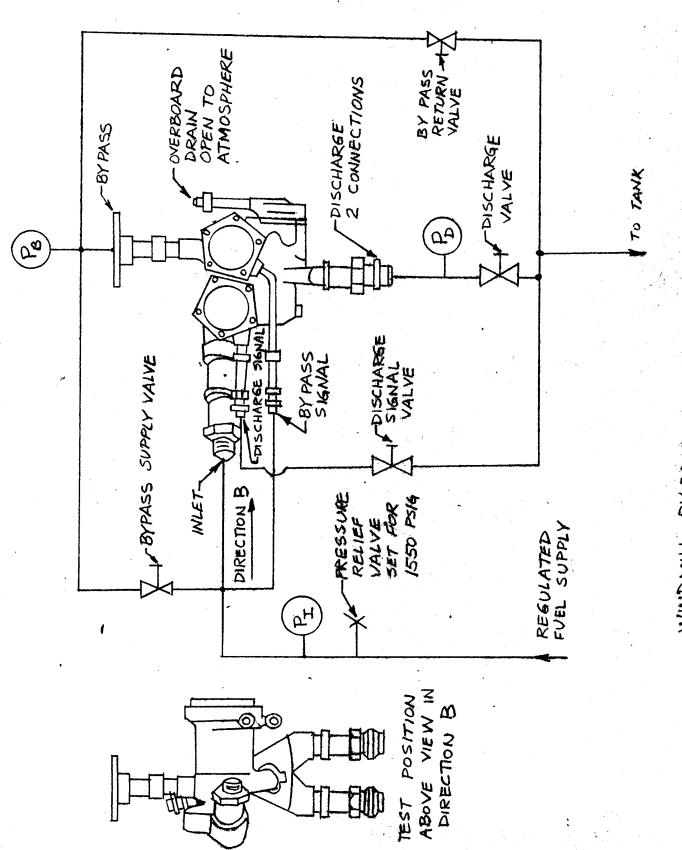
WINDSOR LOCKS, CONNECTICUT, U. S. A.

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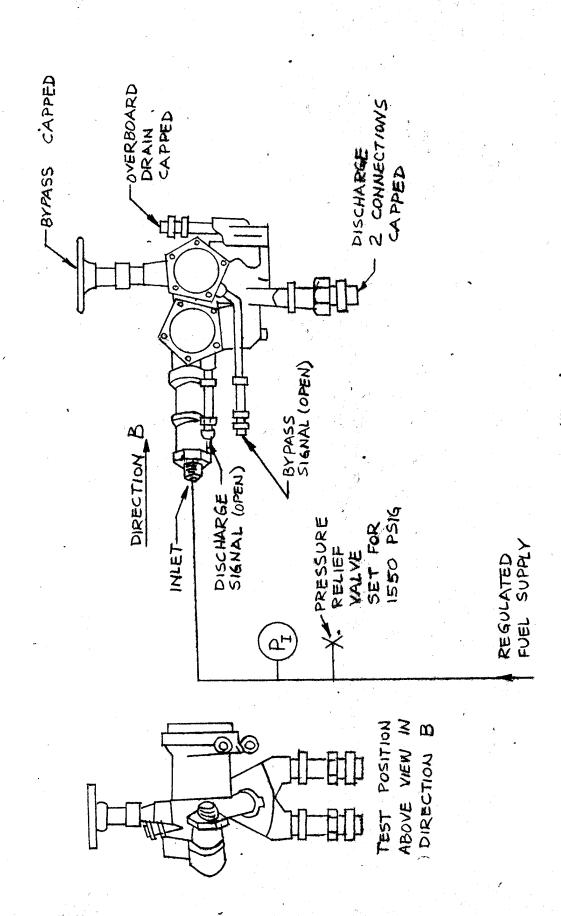
- With the valve, gages, etc. connected as in figure 1, set PI = 400-600 psisopen the discharge signal valve and the bypass return valve. Close the bypass supply valve.

  Adjust PI until the discharge pressure, PD, is equal to 1100 ± 50 psig and inlet pressure is equal to 1100 ± 100 psig. Open the bypass supply valve and close the bypass return valve until bypass pressure, PB, is equal to 110 ± 5 psig.

  Record PI, PD, and PB and any external leakage over a five (5) minute
- \*3.4.2 With the same installation as in 3.4.1, open the bypass return valve, close the bypass supply valve, close the discharge signal valve, and close the discharge valve. Set PI equal to 1100 ± 50 psig. Record PI and any external leakage over a five (5) minute period. There shall be no external leakage over the five (5) minute period.
- 4.0 PRESERVATION AND STORAGE
- After completion of testing, the windmill bypass, check and dump valve assembly shall be drained of fuel and prepared for storage in accordance with HS spec. 1613. Protection covers and containers shall be used to prevent damage or contamination of the assembly.



ASSEMBLY BY PASS, CHECK & DUMP VALVE DIAGRAM SCHEMATIC WINDMILL



BYPASS, CHECK & DUMP VALVE THANK

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# HAMILTON STANDARD : DIVISION OF UNITED AIRCRAFT CORPORATION WINDSON LOCKS, CONNECTION

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Date:	10-11	-62

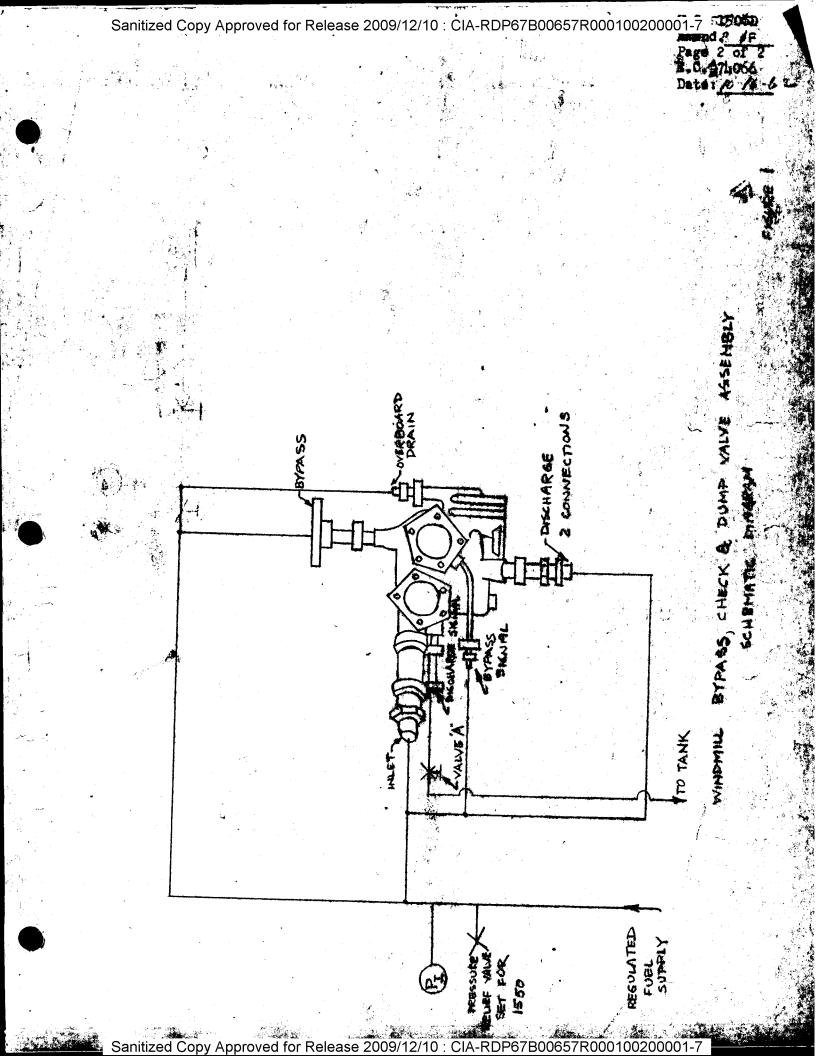
H.S. 1506D CALIBRATION SCHEDULE FOR THE JFC47 WINDMILL BY-PASS, CHECK AND DUMP VALVE, ASSEMBLY P/N 571405 AND 576497

Amendment /

- 1. Change paragraph 3.4.1 from:
  - with the valve, gages, etc. connected as in figure 1, set PI = 100-600 psig. Open the discharge signal valve and the bypass return valve. Close the bypass supply valve. Adjust PI until the discharge pressure, PD, is equal to 1100 ± 50 psig and inlet pressure is equal to 1100 ± 160 psig. Open the bypass supply valve and close the bypass return valve until bypass pressure, PB, is equal to 110 ± 5 psig. Record PI, PD, and PB and any external leakage over a five (5) minute period.

to read:

- #3.4.1 With valve, gages, etc. connected as in Figure 1, open valve A and increase pressure PI to 300 PSI. Close valve A and slowly increase pressure to 1100 ± 50 psi. Hold at this pressure for ten (10) minutes. Then carefully inspect for external leakage all over the control surface.
- 3. Delete paragraph 3.4.
- 4. Replace Fig. 1 with attached Fig. 1.



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R.S. 15069 Amend. Page 1 of 1 E.O. 73697 Date: //- Z-G-2

H.S. 1506D "CALIBRATION SCHEDULE FOR THE JFCL7 WINDMILL BYPASS, CHECK & DUMP VALVE ASSEMBLY P/N 571405 & 576497"

Amendment 2

- 1. Change paragraph 3.4.1 from:
  - 3.4.1 With valve, gages, etc. connected as in Figure 1, open valve.

    A and increase pressure PI to 300 PET. Close valve A and slowly increase pressure to 1100 ± 50 psi W Hold at this pressure (10) minutes. Then carefully inspect for external leakage all over the control surface.

to read:

NWith the valves, gages, etc. connected as in figure 1, open valve A and increase pressure PI to 300 psig. Close valve and slowly increase pressure PI to 1100 i 50 psig. Record PI. Hold at this pressure for ten (10) minutes, derefully inspecting for external leakage all over the control surface. There shall be no external leakage over the ten (10) minute period.

#### MANIETON STANDARD DIVISION OF WHITED AIRCRAFT OSEPONATION WINDSOR LOGUE, CONNECTION

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H. S. 1506D "CALIBRATION SCHEDULE FOR THE JFCLT WINDMILL BY-PASS, CHECK AND DUMP VALVE, ASSEMBLY P/N 571405 AND 576497"

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	_ 7 .		11 100 100	
America				
_				
		- 1. ·		

1. Change paragraph 3.1.3 from:

#### My.1.3 Test Point I

Upon completion of the shimming of this valve, set and record the following conditions:

					LIM	1		LIL		ě
WPD	PDS	PO	P2		W	<b>.</b>		. 71		,
MAN TO		A.E.,	-	•	-	-	~ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	3.70		
975-1025	25-35	50-5	5 40-	<b>K</b> O	80-1	200		107		5
<b>メインキエレモコ</b>	67 <b>-</b> 32		9 407	24	- W			April 1 East	C 100 C 16	d

Record the leakage from the bypass standpipe, leakage from the over-

to read:

### \*#3.1.3 Test Point I:

Upon completion of the shimming of this valve, set and record the following conditions:

WFD	PDS	<u>PD</u> _	<u> 22</u>	WES NY PS
975-1025	25-35	50-55	40-50	80-200 107-113 125-15

Record the leakage from the bypass standpipe, leakage from the overboard drain, and external leakage ever a five (5) minute period."

2. Change paragraph . i. L. from:

### \*\*3.1.4 Test Point II

Increase the dispheree flow to 1675-1725 pph and then to 34,500-35,500 pph aet and record the following conditions:

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E. C. 1506D "CALIBRATION SCHEDULE FOR THE JEOUT WINDMILL BY-PASS, CHECK AND DUMP VALVE, ASSEMBLY P/N 571405 AND 576497"

# A-1-1-2 3

2. (continued)

44 14			LIMIT LIMIT LIMIT
SPEC	WFD	PDS	70 R WS P1 P3
1	1675-1725	170-180	160-170 W-50 80-200 107-113
S	34,550-35,450	160-170	480-520 40-50 4 LO Max

Record the leakage from the bypass standpipe, leakage from the overbeard drain, and external leakage over a five (5) minute period. Leakage from the bypass standpipe shall not exceed 5 cc per minute at test points 2 and II. Leakage from overboard drain shall not exceed 50 cc/min for 1000 pph and 50-55 PD test point I and 1 cc/min at test point II. There shall be external leakage at each test point.

to reads

### "" .i.l Test Point II

Increase the discharge flow to 1675-1725 pph and them to 34,500-35,500 pph set and record the following conditions:

9720	WFD	PDS	PD P2 WIS P1 P3 P4
7	1675-1725	170-180	160-170 40-50 80-200 107-113 270-30
2	24,650-15,450	160-170	480-520 ho-50 ho max.

Record the leakage from the bypass standpipe, leakage from the overtoated drain, and external leakage over a five (5) minute period. Leakage from the bypass standpipe shall not exceed 5 oc per minute at test points I & Leakage from overboard drain shall not exceed 50 oc/min for 1000 ppe and 50-55 PD test point I and I co/min at test point II. There shall be no external leakage at each test point."

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H. S. 1506D "CALIBRATION SCHEDULE FOR THE SFCLT WINDMELL BY-PASS, CHECK AND DUMP VALVE, ASSEMBLY P/N 5711105 AND 576497"

Amondaons 3

Change paragraph 3.1.5 from:

"3.1.5 With the installed per Figure 4 set Fds = 30 ± 5 psig, Fus = 200 ± 10 psig, Fi 80 ± 10 psig, and Pd 55 ± 5 psig. From this condition set up the following test points in the order shelm using test stand inlet control valve and the discharge control valve.

Note: Care should be taken not to overshoot the test points (it may take two or three practice runs before taking final test data).

Record: Inlet press. Pl, discharge press. Rd., fuel flew Wf, and dump overboard valve leakage.

Test Point	Wf pph	Pd psig Leekage Sing be design
1	1.000 ± 25	50-55 50 Max. 19
2	1700 ± 25	160-170 1 Max

3 With the discharge valve closed and the bleed valve open regulate the discharge pressure at 120 ± 10 paig with the inlet by pais valve.

Now reduce the inlet flow slowly by opening the inlet by spass valve and observing the discharge pressure (Pd) at which the dums valve opens. For a more accurate reading hesitate at 20 paig Pd to determine if the pressure will bleed down through the bleed valve; if the pressure will not bleed down carefully open by spass until dump valve opens.

## Limit is 12 paig minimum.

Dump valve opening pressure is defined as the pressure at which the flow suddenly increases from the overboard drain and Pd suddenly decreases. If the discharge pressure will not drop below 12 paig due to test stand boost pressure or pressurised tank then the bised in the discharge line will have to be opened to drop the pressure suntil the dump valve opens.

#### MANIETON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, COMMESTIGUT

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M. S. 1506D "CALIBRATION SCHEDULE FOR THE SPELT WINDMILL BY-PASS, CHECK AND THE VALVE. ASSEMBLY P/N 571405 AND 57049."

## Amendment 3

3. (continued)

Change paragraph ?.1.5 to reso:

which the installed per Figure 4 set Pde = 30 ± 5 psig. For psig. Plat 2 10 psig, and Pd 55 ± 5 psig. From this condition set up the following test points in the order shown using test y stand inlet control valve and the discharge control valve.

Note: Care should be taken not to overshoot the test points (it may take two or three practice runs before taking final test data).

Record: Inlet press. Pl, discharge press. Pd., fuel flow Wig and dump overcourd valve leakage.

Test Point	Wf ppn	Pd pal	*	Leakinge	Links,
	2000 2 25	\$ 50-55			Pax.
Ž.	1700 ± 75	100-17	•	1	Max.

With the liarhange valve open and the bleed valve alread requires the discharge pressure at 120 ± 10 peig with the inlet by pass talve.

Now reduce the inter flow electry by opening the inter propage with until PD drops to 40 psig. It pressure remains at 40 psig open bleed valve so that PM drops electry. Observe disch. pressure 33 at which dump valve opens.

#### Limit is 1' paig minimum

Dump value opening pressure is befined at the pressure at which the flow suddenly increases from the overboard drain and Ed addical decreases. It the discharge pressure will not drop below 12 paig due to test stand boost pressure or pressurized tank them the bidge in the discharge line will have to be opened to drop the pressure until the duag value opened.

# DIVISION OF VEITED ALBERT COMPONITION WINDSON LOCKS, COMMENTION

H.A. WORD Dept. 17/65 L.A. 17/65

E. C. 1506D "CALIBRATION SCHEDULE FOR THE JFOUT WINDMILL BY-PASS, CHECK AND DUMP VALVE, ASSEMBLY P/N 571405 AND 576497"

## Ampadments 3

4. Change paragraph 3.2.1 froms

"3.2.1 With the valve, gages, etc connected as in fig. 3, set the faller ing conditions:

Wf	In		. <b>13</b>			PBS	
1675-17	25		7-113			5-35°	
Record	P5.	P5	shall equal	107-13	i3psi"		

to reads

"3.2.1 With the valve, gages, etc connected as in fig. 3, set the

WTB	<b>PB</b>	•		<b>PB3</b>	P4
•			•V		
1675-1725	107-113			25-35	40 <b>-50</b>
Record PS.	PS shall	anual 107.	113 nat. #		

5. Change paragraph 3.2.3 froms

### "3.2.3 Test Pointer

Upon completion of the shimming of this valve set and rebord the following conditions

J.	WIB	PBS PL PS PL
	275-1025	107-113 25-35 40-50 107-113 80-200
apec.	1075-1725 4975-5025	107-113 25-35 40-50 107-113 80-200 107-113 135-150 40-50 107-113

Record the leakage from the discharge standpipes, leakage from the overboard drain, and external leakage over a (5) minute period. Leakage from the discharge standpipe shall not exceed 2 cc perminute at each test point. There shall be no external leakage at each test point.

# DIVISION OF UNITED AIRCRAFT COMPGRATION WINDSON LOCKS, CONNECTION

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H. S. 1506D "CALIBRATION SCHEDULE FOR THE JFC47 WINDRILL BY-PASS, CHECK AND DUMP VALVE, ASSENBLY P/N 571405 AND 576497"

American S

5. (continued) Change paragraph 3.2.3 to read:

#### #3.2.3 Test Points:

Upon completion of the shimming of this valve set and record the following conditions

1 7 F	WfB	<b>P3</b>	PBS		P\$	ri wa
	975 <b>-</b> 1025 1675 <b>-</b> 1725	107 <b>-1</b> 13	25-35 25-35	10-50	107-113	125-155 80-200 125-155 86-200
spec.	4975-5025	107-113	135-150	50-50	107-113	235-270

Record the leakage from the discharge standpipes, leakage from the overboard drain, and external leakage over a (5) minute period. Leakage from the discharge standpipe shall not exceed? 2 cc per minute at each test point. There shall be no external leakage at each test point.

- 6. Replace figure 3 with attached revised figure 3.
- 7. Replace figure 4 with attached revised figure 4.

# HAMIETON STANDARD DIVISION OF UNITED AIRCRAFT COMPORATION WINDSOR LOCKS, CONNECTIGUT

H.S. 1506D Amond. 4 Page 1 of 1 E.C. 74629 Date: //-2/-62

H. S. 1506D "CALIBRATION SCHEDULE FOR THE JFC47 WINDMILL BY-PASS, CHECK & DUMP VALVE, ASSEMBLY P/N 571405 and 576497"

Amendment 4

1. In Amendment #1 to H.S. 1506D, change sentence 3 from "Delete Paragraph 3.4.2."

# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT

H.S. 1506D Amend. 3— Page 1 of ! E.G.A. 74591 Date: // 24-62

H. S. 1506D - CALIBRATION SCHEDULE FOR THE JFC17 WINDMILL BYPASS, CHECK AND DUMP VALVE ASSEMBLY P/N 571405 and 576497"

Amendment	3		<u> </u>	

Add the following sentence to paragraph 2.4:

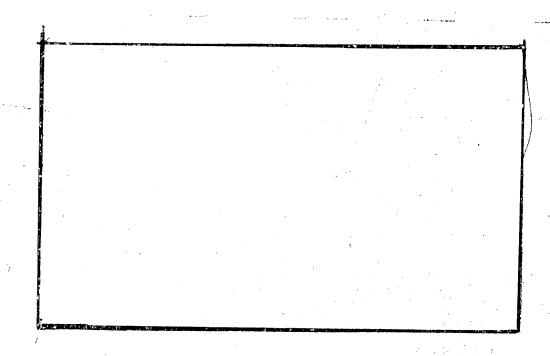
"The test fluid shall contain .ll pounds of P&WA PS67 additive per 50 gallons of fluid."

#### NOTICE:

Add figures 3 & 4 of H.S. Spec. 1506D, Amend 3 and thange pages 1 thru 6 to read 1 thru 8. These pages were inadvertently omitted from amendment when published by Engineering Records.

Flease replace your file copies with the attached sheets.

THANK YOU ENGINEERING RECORDS



# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTIGUT

H.S. 1506D

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Page 1 of 8

E.O. 73702

Date: //-/4-62

REISSUE

H. S. 1506D "CALIBRATION SCHEDULE FOR THE JFCL17 WINDMILL BY-PASS, CHECK AND DUMP VALVE, ASSEMBLY P/N 571405 AND 576497"

## Amendment 3

1. Change paragraph 3.1.3 from:

#### "3.1.3 Fast Point I

Upon completion of the shimming of this valve, set and record the following conditions:

·				LIMIT	LIMIT
WFD	PDS	PD	P2	WfS	PI
975-1025	25-35	50-55	40-50	80-200	107-113

Record the leakage from the bypass standpipe, leakage from the overboard drain, and external leakage over a five (5) minute period.

to reads

## WH3.1.3 Test Point Is

Upon completion of the shimming of this valve, set and record the following conditions:

WFD	FDS	PD	P2	LIMIT	LIMIT	PI	-
975-1025	25-35	50-55	4c-50	80-200	107-113	125-155	

Record the leakage from the bypass standpipe, leakage from the overboard drain, and external leakage over a five (5) minute period."

## 2. Change paragraph 3.1.4 from:

## W#3.1.4 Test Point II

Increase the discharge flow to 1675-1725 pph and then to 34,500-35,500 pph set and record the following conditions:

## DIVISION OF GHITED ALEGEATT CORPORATION WINDSON LOCKS, CONNECTION

H.S. 1506D Exend. 3 Rage 2 of 8 E.C. 73707 Date: //-/4-62 REISSUE

H. C. 1506D "CALIBRATION SCHEDULE FOR THE JFC47 WINDMILL BY-PASS, CHECK AND DUMP VALVE, ASSEMBLY P/N 571405 AND 576497"

## Amendment 3

2. (continued)

SPEC	WFD	PDS	PD	PZ WfS PA P3
1	1675-1725	170-180	160-170	40-50 80-200 107-113
2 .	34.550-35.450	160-170	h80-520	10-50

Record the leakage from the bypass standpipe, leakage from the overboard drain, and external leakage over a five (5) minute period. Leakage from the bypass standpipe shall not exceed 5 cc per minute at test points I and II. Leakage from overboard drain shall not exceed 50 cc/min for 1000 pph and 50-55 PD test point I and I cc/min at test point II. There shall be no external leakage at each test point."

to reads

### "#3.1.4 Test Point II

Increase the discharge flow to 1675-1725 pph and then to 34,500-35,500 pph set and record the following conditions:

SPEC	WFD	PDS	PD	P2	LIMIT LIMIT LIMIT WIS PI P3 PI	
I	1675-1725	170-180	160-170	40-50	80-200 107-113 270-300	
2	311,550-35.450	160-170	L80~520	70-20	TO MAY	

Record the leakage from the bypass standpipe, leakage from the overboard drain, and external leakage over a five (5) minute period. Leakage from the bypass standpipe shall not exceed 5 cc per minute at test points I & II. Leakage from overboard drain shall not exceed 50 cc/min for 1000 pph and 50-55 PD test point I and I cc/min at test point II. There shall be no external leakage at each test point."

# HAMILION STANDARD DIVISION OF UNITED AIRCRAFT COMPORATION WINDSOR LOCKS, CONNECTICUT

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H. S. 1506D "CALIBRATION SCHEDULE FOR THE JFC47 WINDMILL BY-PASS, CHECK AND DUMP VALVE, ASSEMBLY P/N 571405 AND 576497"

# Amendment 3

## 3. Change paragraph 3.1.5 from:

With the installed per Figure 4 set Pds = 30 ± 5 psig, Pbs = 200 ± 10 psig, Pl 80 ± 10 psig, and Pd 55 ± 5 psig. From this condition set up the following test points in the order shown using test stand inlet control valve and the discharge control valve.

Note: Care should be taken not to overshoot the test points (it may take two or three practice runs before taking final test data).

Record: Inlet press. Pl, discharge press. Pd., fuel flow Wf, and dump overboard valve leakage.

Test Point	Wf pph	Pd psig	Les	akage Limit c	e/min.
1	1000 ± 25	50-55		50 Max.	
2	1700 ± 25	160-170		l Max.	

3 With the discharge valve closed and the bleed valve open regulate the discharge pressure at 120 ± 10 psig with the inlet by-pass valve.

Now reduce the inlet flow slowly by opening the inlet by-pass valve and observing the discharge pressure (Pd) at which the dump valve opens. For a more accurate reading hesitate at 20 psig Pd to determine if the pressure will bleed down through the bleed valve; if the pressure will not bleed down carefully open by-pass until dump valve opens.

## Limit is 12 psig minimum.

Dump valve opening pressure is defined as the pressure at which the flow suddenly increases from the overboard drain and Pd suddenly decreases. If the discharge pressure will not drop below 12 psig due to test stand boost pressure or pressurized tank then the bleed in the discharge line will have to be opened to drop the pressure until the dump valve opens."

# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTIGUT

H.S. 1506D Amend. 3 Page: of 8 E.C. 73701 Date://-/4-62 REISSUE

H. S. 1506D "CALIBRATION SCHEDULE FOR THE JPCLT WINDMILL BY-PASS, CHECK AND DUMP VALVE, ASSEMBLY P/N 571405 AND 576497"

# Amendment 3

#### 3. (continued)

Change paragraph 3.1.5 to reads

With the installed per Figure 4 set Pds = 30 ± 5 psig, Phs = 200 ± 10 psig, PI 80 ± 10 psig, and Pd 55 ± 5 psig. From this condition set up the following test points in the order shown using test stand inlet control valve and the discharge control valve.

Note: Care should be taken not to overshoot the test points (it may take two or three practice runs before taking final test data).

Record: Inlet press. PI, discharge press. Pd., fuel flow Wi, and dump overboard valve leakage.

Test Point	Wf cph	Pd psig	Leakage Limit co/mic
	1000 ± 25	50-55	50 Max.
2	1700 ± 25	1.60-170	1 Max.

3 With the discharge valve open and the bleed valve closed regulate the discharge pressure at 120 ± 10 psig with the inlet by-pass valve.

Now reduce the inlet flow slowly by opening the inlet by-pass valve until PD drops to h0 paig. If pressure remains at 40 paig, open bleed valve so that PD drops slowly. Observe disch. pressure PD at which dump valve opens.

## Limit is 12 page minisum.

Dump valve opening pressure is defined at the pressure at which the flow suddenly increases from the overboard drain and Pd suddenly decreases. If the discharge pressure will not drop below 12 poig due to test stand boost pressure or pressurized tank then the bleed in the discharge line will have to be opened to drop the pressure until the dump valve opens."

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# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSON LOCKS, CONNECTIGUT

H.S. 1506D

Amend. 3

Page 5 of 8

E.C. 73702

Date: //-/4-62

REISSUE

H. S. 1506D "CALIBRATION SCHEDULE FOR THE JFC47 WINDMILL BY-PASS, CHECK AND DUMP VALVE, ASSEMBLY P/N 571405 AND 576497"

### Amendment 3

4. Change paragraph 3.2.1 from:

With the valve, gages, etc connected as in fig. 3, set the following conditions:

Wf In	PB -	PBS	P4
1675-1725	107-113	25-35	40-50
Record P5.	P5 shall equal	107-113ps1"	

to read:

With the valve, gages, etc connected as in fig. 3, set the following conditions

WTB	PB		PBS	Pi4
1675-1725 Record P5.	107-113 P5 shall equal	107-113 psi."	25-35	40-50

5. Change paragraph 3.2.3 froms

## "3.2.3 Test Points:

Upon completion of the shimming of this valve set and record the following condition:

	WfB	PB		PBS PL		701.	Limit		mitte	ACCORDANGE AND	
		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1						Fo		WL'3	
	975-1025 1675-1725	107-113 107-113		25 <b>-</b> 35 25-35		40-50		107-113	100 100 100 100 100 100 100 100 100 100	80-200	
apac.	4975-5025	107-113	1	L35-150	1 f	40-50		107-113			

Record the leakage from the discharge standpipes, leakage from the overboard drain, and external leakage over a (5) minute period. Leakage from the discharge standpipe shall not exceed 2 cc per minute at each test point. There shall be no external leakage at each test point."

#### HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION— WINDSOR LOCKS, CONNECTICUT

H.S. 1506D

Amond. 3

Page 6 of 8

E.C. 73701

Date: //-/4-62

REISSUE

H. S. 1506D "CALIBRATION SCHEDULE FOR THE JFC17 WINDMILL BY-PASS, CHECK AND DUMP VALVE, ASSEMBLY P/N 571405 AND 576497"

# Amendment\_3

5. (continued) Change paragraph 3.2.3 to read:

#### 13.2.3 Test Points:

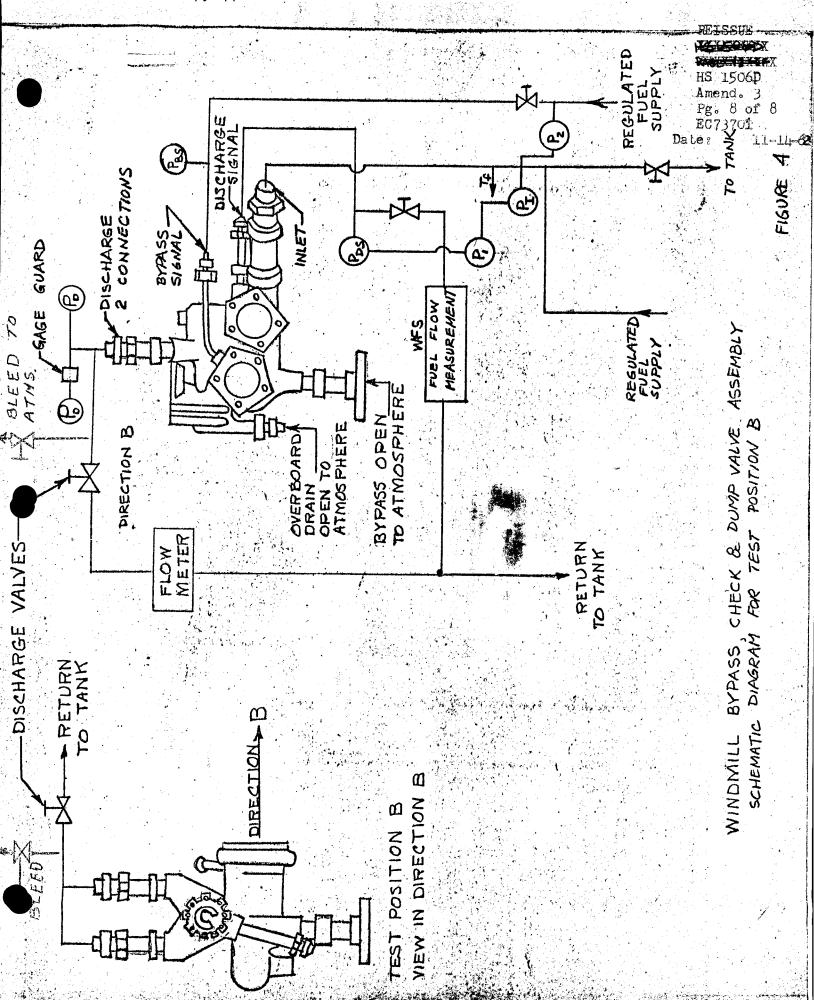
Upon completion of the shimming of this valve set and record the following conditions

. ,	WfB	PB	PBS	Pl	P5 -	PI	WIS
spec	975-1025 1675-1725 1975-5025	107-113 107-113 107-113	25-35 25-35 135-150	40-50 40-50 50-50	107-113 107-113 107-113	125-155	80-200 80-200

Racord the leakage from the discharge standpipes, leakage from the overboard drain, and external leakage over a (5) minute period. Leakage from the discharge standpipe aball not exceed 2 oc per minute at each test point. There shall be no external leakage at each test point."

- 6. Replace figure 3 with attached revised figure 3.
- 7. Replace figure 4 with attached revised figure 4.

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HSF-755.1A 5/61

# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT, U. S. A.

CODE IDENT NO. 73030 PAGE - 2 OF

SCOPE 1.0

- This specification covers the method of testing and calibrating the JFC-47 Interim Bypass Valve Assembly. 1.1
- GENERAL REQUIREMENT 2.0
- Equipment Requirement 2.1
- Flowbench capable of supplying at least 1000 to 35,000 PPH fuel flow at 2.1.1 900 psig pressure.
- Boost Pump capable of maintaining the stand fuel pump inlet pressure at 25 15 psig over a fuel flow range of 1000 to 35,000 PPH. 2.1.2
- Heat Exchanger to maintain the fuel temperature at the valve assembly inlet within the range of 70° to 110°F. 2.1.3
- Filter containing 25 to 40 micron element installed in the stand pump 2.1.4 discharge line.
- Test fitting 544900-ET-33, to adapt to valve assembly standpipes. 2.1.5
- Installation 2.2
- The valve assembly shall be mounted on the flow bench, and installed per 2.2.1 Figure 1 or 2 as applicable.
- Instrumentation for taking the measurements listed below with the 2.3 accuracy specified.
- Pressure Gages 2.3.1
  - PI Inlet pressure, at least 30 1500 psig pressure range with an accuracy of ± 5 psig within this range.
  - PD Discharge pressure, at least 50 1500 paig pressure range with an accuracy of ± 5 psig within this range.
  - PS Signal pressure, at least 50 600 psig pressure range with an accuracy of ± 3 psig within this range.
  - △ Pl Inlet Press minus signal press. (Fl-Ps) at least 0-150 psi pressure range with an accuracy of ±.5% in the range of 107-113 psi.
  - △P2' Inlet Press minus discharge press (P1-Pd) at least 0-50 psi press range with an accuracy of 5% in range of 25 psi.
  - Fuel Flow Meter 2.3.2
    - WFD Discharge fuel flow, at least 1000 35,000 PFH fuel flow range with an accuracy of ± 1% within this range.
  - Fuel Temperature, measure at valve assembly inlet with at least a 70° to 110 F temperature range, with an accuracy of ±2 F within this range. 2.3.3

HSF-755.1A 5/61

#### HAMILTON STANDARD

## SPEC. NO. HS 15888

# DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTICUT, U. S. A.

CODE	IDENT	NO.	73030	
PAGE	3	OF		

2.4 Test Fluid shall be PW 523B or PMC9073.

2.5 Data to be recorded

2.5.1 The following data should be recorded on each data sheet:

Valve Assembly Serial Number Valve Assembly Part Number Fuel Type and Specific Gravity Fuel Inlet Temperature

2.5.2 The following data shall be recorded when specified:

 $\triangle PL - (Pl-Ps)$ 

Pl - Inlet Pressure

PD - Discharge Pressure

PS - Signal Pressure

WfD - Discharge Fuel Flow

 $\triangle PD - (PI - PD)$ 

#### 3.0 TEST REQUIREMENTS

- 3.1 Connect the line valves and gages as shown in Figure 2 for 577911. Regulate the signal supply valve to obtain 25-35 psi and open the discharge valve. Regulate the inlet valve to obtain a fuel flow of 1150 ± 50 PFH with PD set at 70 ± 5 and record the differential pressure (Pl PS). The differential pressure ΔPl should be 110 ± 3 psi. Repeat at a fuel flow of 1700 ± 25 pph, with Ps at 172 to 182 psig and PD at 202 ± 10 psig. ΔPl should be 110 ± 5 psi. For 577162 valve connect line as shown in Fig 1. Regulate PBS t. 172-182 psig and WfD to 1700 ± 25. ΔPl should be 110 ± 3 psi.
- 3.2 In order to bring the differential pressure, PI PS, within the limits of 110 ± 3 psi, add or subtract shims, P/N 553130, as found necessary.
- 3.3 With 577911 valve install as in fig 2, and Signal Pressure (PS) set at 167 ± 15 psig, PD at 510 ± 15 psig pass 35,000 ± 500 PPH fuel flow through the valve. Record Inlet Pressure (PI) and Discharge Pressure (PD). AP2 shall not exceed 40 psi. For 577162 Valve set PBs = 135 150, PD at 48 ± 2 psi and pass 5000 pph through the valve. Record P1, PD. No A P limit.
- 3.4 With conditions as in 3.3, raise Signal Pressure (PS) up to 45 ± 5 psig greater than inlet Pressure (PT) by opening up the signal supply valve and measure leakage out of the discharge standpipe. Maximum allowable leakage is 5 cc/min.
- 3.5 With discharge, and signal press connections interconnected apply 1100 ± 50 psig to the inlet and signal connections. There shall be no external leakage over a five (5) minute period.

3.6 Disconnect inlet supply line and apply 135 ± 5 psig and 540 ± 20 psig. At each point measure the leakage from PD. Maximum leakage should not exceed 2 cc/min.

4.0 PRESERVATION AND STORAGE

4.1 After completion of testing, the Interim Bypass Valve shall be drained of fuel and prepared for storage in accordance with H.S.Spec. 1613 as applicable. Protection covers and containers shall be used to prevent damage or contamination of the assembly.

5.0 APPLICABLE FIGURES
Figure I & 2. Schematic diagram for valve operation.

# HAMILTON STANDARD DIVISION OF UNITED AIRCRAFT CORPORATION WINDSOR LOCKS, CONNECTION

H.S. 1582A

Amend. /
Page 1 of 1:
E.C. Elihhoh

Date: 6-5-62

H.S. 1582A "CALIBRATION SCHEDULE FOR THE JFCL? INTERIM BYPASS VALVE ASSY P/N577162
AND INTERIM SOV, 577163 & 577911"

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Amendment	,		•
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		<b>_</b>	

- 1. Change para 3.1 from:
  - 3.1 "Connect the line valves and gages as shown in Figure 2 for 577911.

    Regulate the signal supply valve to obtain 172-182 psi and open the discharge valve. Regulate the inlet valve to obtain a fuel flow of 1150 ± 50 PPH with PD set at 202 ± 10 and record the differential pressure (PI PS). The differential pressure ΔP2 should be 110 ± 3 psi. For 577162 valve connect line as shown in Fig 1. Regulate PDS to 25-35 psig and WfD to 1700 ± 25. Δ P2 should be 110 ± 3 psi.

to read:

- "Connect the line valves and gages as shown in Figure 2 for 577911. Regulate the signal supply valve to obtain 172-182 psi and open the discharge valve. Regulate the inlet valve to obtain a fuel flow of 1150 ± 50 PPH with PD set at 202 ± 10 and record the differential pressure (PI PS). The differential pressure  $\triangle$ Pl should be 110 ± 3 psi. For 577162 valve connect line as shown in Fig 1. Regulate PDS to 25-35 psig and WfD to 1700 ± 25.  $\triangle$  Pl should be 110 ± 3 psi."
- 2. Change para. 3.3 from:

"With 577911 valve install as in fig 2, and Signal Pressure (PS) set at 167±15 psig, pass 35,000 ± 500 PPH fuel flow through the valve. Record Inlet Pressure (PI) and Discharge Pressure (PD). API shall not exceed 40 psi. For 577162 Valve set Ps = 135-150 and pass 5000 pph through the valve. Record Pl, Pd. No AP limit."

to read:

"With 577911 valve install as in fig 2, and Signal Pressure (PS) set at 167 ± 15psig, pass 35,000 ± 500 PPH fuel flow through the valve. Record Inlet Pressure (PI) and Discharge Pressure (PD). A P2 shall not exceed 40 psi. For 577162 Valve set Ps = 135-150 and pass 5000 pph through the valve. Record P1, PD. No A P limit."

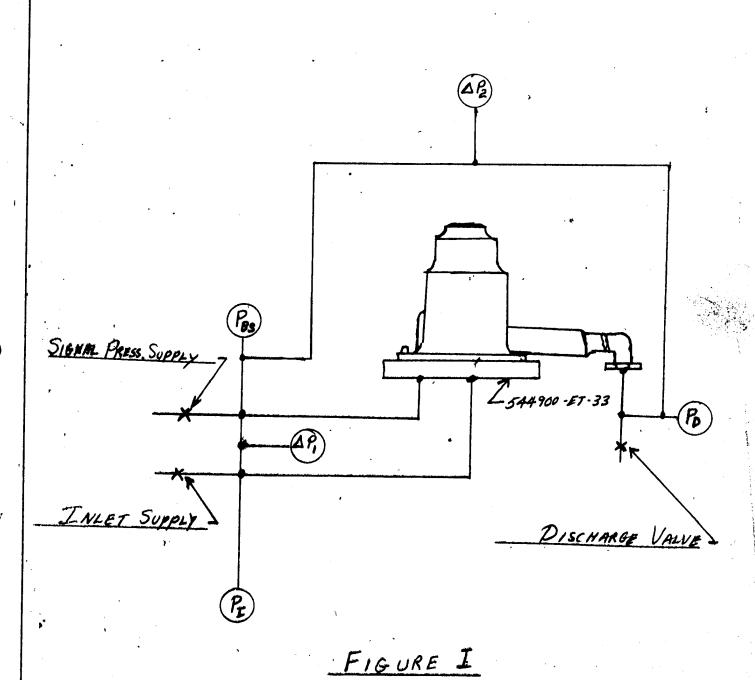
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JFC-47 BYPASS VALUE
577162

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SIGNAL PRESS SUPPLY 1.5449NO-E7-33 DISCHARGE VALVE INLET SUPPLY. FIGURE II JFC-47 MIN PRESS SOV

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